### GATE CIVIL ENGINEERING 2008 (CE)

### 1 to 20 carry one mark each

The product of matrices (PQ) P is

	(A)	P <sup>-1</sup>	(B)	Q <sup>-1</sup>	(C)	$P^{-1}Q^{-1}$	(D)	PQP <sup>-1</sup>
2	The ger	neral solution of	$\frac{d^2y}{dx^2}$ +	y = 0 is				
	(A) (C)	$y=P \cos x + Q \sin x$ $y = P \sin x$	sin x		(B) (D)	$y=P \cos x$ $y = P \sin^2 x$		
3	are 2 ×		tively. Th without	ne maximum am	ount of		r unit vo	d stress for mild steel dume that can be
4		orced concrete st e to be used as p			ucted al	ong a sea coast.	The min	nimum grade of
	(A)	M 15	(B)	M 20	(C)	M 25	(D)	M 30
5		nical option to sa bundling of bars providing smalle providing larger	tisfy the s er diame diamete		bond is number umber	by	not getti	ng satisfied. The
6	The sha	ape of the cross-	section,	which has a larg	jest shap	oe factor, is		
	(A)	rectangular	(B)	I-section	(C)	diamond	(D)	solid circular
7	Group s	symbols assigned	to silty	sand and clayey	sand a	re respectively		
	(A)	SS and CS	(B)	SM and CS	(C)	SM and SC	(D)	MS and CS
8	When a (A) (B) (C) (D)	retaining wall m Passive earth pr Swelling pressur Pore pressure Active earth pre	ressure re	vay from the bad	:k-fill, th	e pressure exerto	ed on th	e wall is termed as
9	Compa	ction by vibratory	y roller is	s the best metho	d of cor	npaction in case	of	
	(A) (B) (C) (D)	moist silty sand well graded dry clay of medium silt of high com	compres	•				

### GATE CIVIL ENGINEERING 2008 (CE)

10	•	son standing on the bank of a canal drops a stone on the water surface. He notices that the bance on the water in not traveling up-stream. This is because the flow in the canal is								
	(A)	sub-critical	(B)	super-critical	(C)	stead	dy	(D)	unifor	m
11		wave with a kno raph will have	own inflo	ow hydrograph is	s routed	throu	gh a large	reservoir	r. The c	utflow
	(A) (B) (C) (D)	attenuated pea increased peak	k with in with inc	educed time-bas acreased time-bas reased time-base duced time-base	ase se					
12		e channel is to be ean flow velocity	(m/s) in		obtained	by			per Lac	ey's method.
	(A) (C)	$(Qf^2 / 140)^{1/6}$ $(Q^2f^2 / 140)^{1/6}$	)		(B) (D)	(Qf / 0.48	(Q / f) 1/3	9		
13	materia	se width of an el al of the dam is ( el is given by								
		$\frac{b}{H} = \frac{1}{\sqrt{G - K}}$	(B)	$\frac{b}{H} = \sqrt{G - K}$	(C)	$\frac{b}{H} =$	$\frac{1}{G-K}$	(D)	$\frac{H}{p} = \frac{K}{k}$	$\frac{1}{\sqrt{G-K}}$
14	Two pr	imary air polluta	nts are							
	(A) (C)	sulphur oxide a sulphur oxide a			(B) (D)		gen oxide e and perc	•		ylnitrate
15	Two bid	odegradable com	ponents	of municipal so	olid waste	e are				
	(A)	plastics and wo	od		(B)	card	board and	glass		
	(C)	leather and tin	cans		(D)	food	wastes an	d garder	n trimm	ings
16	The spe	ecific gravity of p	paving bi	tumen as per IS	S:73 – 19	992 lie	s between			
	(A)	1.10 and 1.06			(B)	1.06	and 1.02			
	(C)	1.02 and 0.97			(D)	0.97	and 0.92			
17		oined value of fla quence in which		•		be de	etermined	for a sar	nple of	aggregates.
	(A)	elongation inde	x test fo	llowed by flakin	ess inde	x test	on the who	ole samp	le.	
	(B)			owed by elongat				•		
	(C) (D)			owed by elongat Illowed by flakin				, ,		
	(D)	elongation inde	x test to	niowed by nakin	ess inde	x test	on non-eio	ingateu a	aggrega	nes.
18		pacities of "One- er hour, with no ively			**		•		•	
	(A)	1200 and 2400			(B)	1800	and 2000			
	(C)	1200 and 1500			(D)	2000	and 1200			

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19	The sh	The shape of the STOP sign according to IRC: 67-2001 is							
	(A) (C)	circular octagonal			(B) (D)	triangular rectangular			
20	The ty (A) (C)	pe of surveying Geodetic surve Preliminary su	eying	the curvature o	f the ear (B) (D)	rth is taken into Plane surveyir Topographical	g		
			2	21 to 75 carry t	two ma	rks each			
21	The e	quation $k_1 \frac{\partial^2 h}{\partial x^2}$	$+k_z \frac{\partial^2 h}{\partial z^2}$	= 0 can be trar	nsformed	d to $\frac{\partial^2 h}{\partial x_1^2} + \frac{\partial^2 h}{\partial z^2}$	= 0 by s	ubstituting	
	(A)	$x_1 = x \frac{k_z}{k_x}$			(B)	$x_1 = x \frac{k_x}{k_z}$ $x_1 = x \sqrt{\frac{k_z}{k_x}}$			
	(C)	$x_1 = x \frac{k_z}{k_x}$ $x_1 = x \sqrt{\frac{k_x}{k_z}}$			(D)	$x_1 = x \sqrt{\frac{k_z}{k_x}}$			
22.	The va	alue of $\int_{0.0}^{3.x} (6-x)^{3}$	– y) dx	dy is	9				
	(A)	13.5	(B)	27.0	(C)	40.5	(D)	54.0	
23				be fitted in a str $\Sigma x^2 = 14$ and $\Sigma xy$				the method of le	ast
	(A)	2 and 3	(B)	1 and 2	(C)	2 and 1	(D)	3 and 2	
24	Solutio	on of $\frac{dy}{dx} = -\frac{x}{y}$	at $x = 1$	and $y = \sqrt{3}$ is $x+y^2 = 4$					
	(A)	$x-y^2=2$	(B)	$x+y^2=4$	(C)	$x^2-y^2=-2$	(D)	$x^2+y^2=4$	
25	f(x) = = 0 fc	$x^2$ for $-1 \le x \le x$ or any other value	1, and e of x	of a random varia					
	Then,	the percentage	probabil	ity P $\left(-\frac{1}{3} \le x \le \frac{1}{3}\right)$	$\left(\frac{1}{3}\right)$ is				
	(A)	0.247	(B)	2.47	(C)	24.7	(D)	247	
26	The E	igen values of th	e matrix	$x[P] = \begin{bmatrix} 4 & 5 \\ 2 & -5 \end{bmatrix}$					
	(A)	-7 and 8	(B)	-6 and 5	(C)	3 and 4	(D)	1 and 2	
27	private of whi	e car is 0.45. Wh ch the probabilit	ile using y of con	the public trans	sport, fur s is 0.55.	rther choices ava In such a situat	ilable ar ion, the	robability of using e bus and metro, probability (round	out
	(A)	0.45, 0.30 and			(B)	0.45, 0.25 and			

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The following simultaneous equations

x+y+z=3

x+2y+3z=4

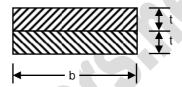
x+4y+kz=6

will NOT have a unique solution for k equal to

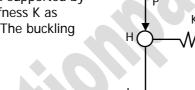
(A)

- (B) 30
- (C) 6
- (D) 7
- The inner (dot) product of two vectors  $\vec{P}$  and  $\vec{Q}$  is zero. The angle (degrees) between the two vectors is
  - (A) 0
- (B) 5
- (C) 90
- (D) 120

30 Cross-section of a column consisting of two steel strips, each of thickness t and width b is shown in the figure below. The critical loads of the column with perfect bond and without bond between the strips are P and  $P_0$  respectively. The ration  $P/P_0$  is



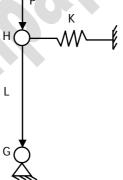
- (A)
- (B)
- 4
- (C) 6
- (D) 8
- A rigid bar GH of length L is supported by a hinge and a spring of stiffness K as shown in the figure below. The buckling load, P<sub>cr'</sub> for the bar will be



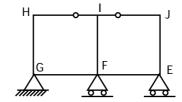
(A) 0.5 KL

2

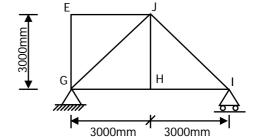
- (B) 0.8 KL
- (C) 1.0KL
- (D) 1.2KL



- The degree of static indeterminacy of the rigid frame having two internal hinges as shown in the figure below, is
  - (A) 8
  - (B) 7
  - (C) 6
  - (D) 5



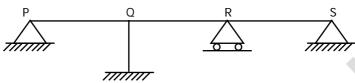
33 The members EJ and IJ of a steel truss shown in the figure below are subjected to a temperature rise of 30°C. The coefficient of thermal expansion of steel is 0.000012 per °C per unit length. The displacement (mm) of joint E relative to joint H along the direction HE of truss, is



- (A) 0.255
- (B) 0.589
- (C) 0.764
- (D) 1.026

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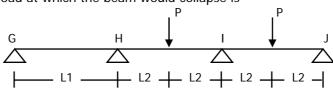
- The maximum shear stress in a solid shaft of circular cross-section having diameter subjected to a torque T is  $\tau$ . If the torque is increased by four times and the diameter of the shaft is increased by two times, the maximum shear stress in the shaft will be
  - (A) 21
- (B)
- C) t /2
- (D) t /-
- 35 The span(s) to be loaded uniformly for maximum positive (upward) reaction at support P, as shown in the figure below, is (are)



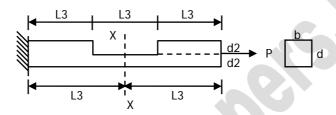
- (A) PQ only
- (B) PQ and QR
- (C) QR and RS
- (D) PQ and RS
- A vertical PQ of length L is fixed at its top end P and has a flange to the bottom end A weight W is dropped vertically from a height h (<L) on to the flange. The axial stress in the rod can be reduced by
  - (A) increasing the length of the rod
  - (B) decreasing the length of the rod
  - (C) decreasing the area of cross-section of the rod
  - (D) increasing the modulus of elasticity of the material
- Un-factored maximum bending moments at a section of a reinforced concrete beam resulting from a frame analysis are 50, 80, 120 and 180kNm under dead, live, wind and earthquake loads respectively. The design moment (kNm) as per IS: 456- 2000 for the limit state of collapse (flexure) is
  - (A) 195
- (B) 250
- (C) 345
- (D) 372
- A reinforced concrete column contains longitudinal steel equal to 1 percent of net cross-sectional area of the column. Assume modular ration as 10. the loads carried (using the elastic theory) by the longitudinal steel and the net area of concrete, are  $P_s$  and  $P_c$  respectively. The ration  $P_s/P_c$  expressed as percent is
  - (A) 0.1
- (B) 1
- (C) 1.1
- (D) 10
- A pre-tensioned concrete member of section  $200 \text{mm} \times 250 \text{mm}$  contains tendons of area  $500 \text{ mm}^2$  at the centre of gravity of the section. The pre-stress in tendons is  $1000 \text{N/mm}^2$ . Assuming modular ratio as 10, the stress (N/mm<sup>2</sup>) in concrete is
  - (A) 11
- (B) 9
- (C)
- (D) !
- Rivets and bolts subjected to both shear stress ( $\tau_{vf, cal}$ ) and axial tensile stress ( $\sigma_{tf, cal}$ ) shall be so proportioned that the stresses do not exceed the respective allowable stresses  $\tau_{vf}$  and  $\sigma_{tf}$ , and the value of  $\left(\frac{\tau_{vf, cal}}{\tau_{vf}} + \frac{\sigma_{tf, cal}}{\sigma_{tf}}\right)$  does not exceed
  - (A) 1.0
- (B) 1.2
- (C) 1.4
- (D) 1.8

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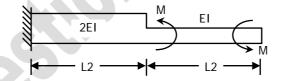
A continuous beam is loaded as shown in the figure below. Assuming a plastic moment capacity equal to MP, the minimum load at which the beam would collapse is



- (A)  $\frac{4M_p}{L}$
- (B)  $\frac{6M_p}{I}$
- (C)  $\frac{8M_p}{I}$
- (D)  $\frac{10M_p}{L}$
- The maximum tensile stress at the section X X shown in the figure below is



- (A)  $\frac{8P}{bd}$
- (B)  $\frac{6P}{bd}$
- $\frac{4P}{bd}$
- (D)  $\frac{2P}{bd}$
- The stepped cantilever is subjected to movements, M as shown in the figure below. The vertical deflection at the free end (neglecting the self weight) is
  - (A)  $\frac{ML^2}{8EI}$
  - (B)  $\frac{ML^2}{4EI}$
  - (C)  $\frac{ML^2}{2EI}$
  - (D) Zero



- The liquid limit (LL), plastic limit (PL) and shrinkage limit (SL) of a cohesive soil satisfy the relation
  - (A) LL>PL<SL
- (B) LL>PL>SL
- (C) LL<PL<SL
- (D) LL<PL>SL
- A footing  $2m \times 1m$  exerts a uniform pressure of  $150kN/mm^2$  on the soil. Assuming a load dispersion of 2 vertical to 1 horizontal, the average vertical stress  $(kN/m^2)$  at 1.0m below the footing is
  - (A) 50
- (B) 75
- (C) 80
- (D) 100
- A direct shear test was conducted on a cohesion-less soil (c=0) specimen under a normal stress of 200kN/m<sup>2</sup>. The specimen failed at a shear stress of 100kN/m<sup>2</sup>. The angle of internal friction of the soil (degrees) is
  - (A) 26.6
- (B) 29.5
- (C) 30.0
- (D) 32.6
- A pile of 0.50m diameter and length 10m is embedded in a deposit of clay. The undrained strength parameters of the clay are cohesion =  $60kN/m^2$  and the angle in internal friction = 0. The skin friction capacity (kN) of the pile for an adhesion factor of 0.6, is
  - (A) 671
- (B) 565
- (C) 283
- (D) 106

#### GATE CIVIL ENGINEERING 2008 (CE)

48	A saturated clay stratum draining both at the top and bottom undergoes 50 percent consolidation in 16 years under an applied load. If an additional drainage layer were present at the middle of the clay stratum, 50 percent consolidation would occur in							
	(A)	2 years	(B)	4 years	(C)	8 years	(D)	16 years
49	intensit					les by 10mm und sand deposit an		tain loading I to the same load
	(A)	2.0mm	(B)	27.8mm	(C)	3.02mm	(D)	50.0mm
50	from ar		The pun					aquifer, uniformly 102m to 99m. The
	(A)	0.20	(B)	0.30	(C)	0.40	(D)	0.50
51		on a permeable it as per Khosla's			ream sh	eet pile is shown	in the fi	gure below. The exit
	***	_ <u></u>	₩e 5m 10m	Floor	7 <del>-</del> ×××			
		Downstrea	ım sheet	pile				
	(A)	1 in 6.0	(B)	1 in 5.0	(C)	1 in 3.4	(D)	1 in 2.5
52	Water en	nerges from an ogee draulic jump at the t	e spillway v	with velocity = 13.72	m/s and d	epth = 0.3 m at its to	e. The tail	water depth required to
	(A)	6.48m	(B)	5.24m	(C)	3.24m	(D)	2.24m
53	pipe, h	aving equivalent	roughne	ess k <sub>s</sub> as 0.12 mr	n, yields	matic viscosity = s an average she ness of laminar so 6.0	ar stress	
54	in the la	aboratory where	maximu	ım available disc	harge is		geomet	e physically modeled rically similar model del is
	(A)	26.4	(B)	25.0	(C)	20.5	(D)	18.0
55	evapoti					required at this cormly in 20 days		meet the ng other field losses
	is (A)	2.52	(B)	2.31	(C)	2.01	(D)	1.52
56	A waste	ewater sample c	ontains <sup>·</sup>	10 <sup>-56</sup> mmol /I of	OH ior	ns at 25°C. The p	H of this	s sample is
	(A)	8.6	(B)	8.4	(C)	5.6	(D)	5.4

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57. Group I lists estimation methods of some of the water and wastewater quality parameters. Group II lists the indicators used in the estimation methods. Match the estimation method (Group I) with the corresponding indicator (Group II).

	<u> </u>		
	Group I		Group II
P.	Azide modified Winkler	1.	Eriochrome Black T
	method for dissolved oxygen		
Q.	Dichromate method for	2.	Ferrion
	chemical oxygen demand		
R.	EDTA titrimetric method for	3.	Potassium chromate
	hardness		
S.	Mohr or Argentometric	4.	Starch
	method for chlorides		

(A)	D_3	Q-2,	<b>D</b> ₋1	S_1
( , , ,	ı-J,	Q-Z,	11 - 1 ,	J-4

(B) P-4, Q-2, R-1, S-3

(C) P-4, Q-1, R-2, S-3

(B) P-4, Q-2, R-3, S-1

58. Determine the correctness or otherwise of the following Assertion [a] and the Reason [r] **Assertion :** It eliminates backing up of sewage in the incoming smaller diameter sewer.

- (A) Both [a] and [r] are true and [r] is the correct reason for [a]
- (B) Both [a] and [r] are true but [r] is not the correct reason for [a]
- (C) Both [a] and [r] are false
- (D) [a] is true but [r] is false

59. The 5-day BOD of a wastewater sample is obtained as 190 mg/I (with  $k = 0.01h^{-1}$ ). The ultimate oxygen demand (mg/I) of the sample will be

- (A) 3800
- (B) 475
- (C) 271
- (D) 190

60. A water treatment plant is required to process  $28800 \text{ m}^3/\text{d}$  of raw water (density =  $1000 \text{ kg/m}^3$ , kinematic viscosity =  $10^{-6}\text{m}^2/\text{s}$ ). The rapid mixing tank imparts a velocity gradient of  $900\text{s}^{-1}$  to blend 35mg/I of alum with the flow for a detention time of 2 minutes. The power input (W) required for rapid mixing is

- (A) 32.4
- (B) 36
- (C) 324
- (D) 32400

61. Match Group I (Terminology) with Group II (Definition/Brief Description) for wastewater treatment systems

	Group I	Group II			
P.	Primary treatment	1.	Contaminant removal by physical forces		
Q.	Secondary treatment	2.	Involving biological and / or chemical reaction		
R.	Unit operation	3.	Conversion of soluble organic matter to business		
S.	Unit process	4.	Removal of solid materials from incoming wastewater		

(A) P-4, Q-3, R-1, S-2

(B) P-4, Q-3, R-2, S-1

(C) P-3, Q-4, R-2, S-1

(D) P-1, Q-2, R-3, S-4

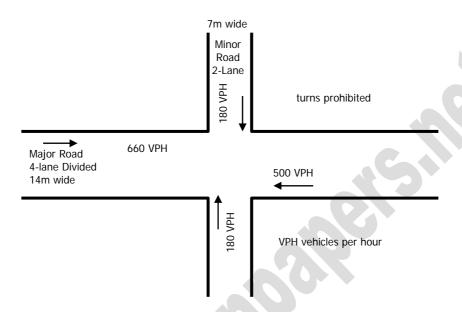
62. A roundabout is provided with an average entry width of 8.4 m, width of weaving section as 14 m, and length of the weaving section between channelizing islands as 35 m. The crossing traffic and total traffic on the weaving section are 1000 and 2000 PCU per hour respectively. The nearest rounded capacity of the roundabout (in PCU per hour is)

- (A) 3300
- (B) 3700
- C) 4500
- (D) 5200

#### GATE CIVIL ENGINEERING 2008 (CE)

63. Design parameters for a signalized intersection are shown in the figure below. The green time calculated for major and minor roads are 34 and 18s respectively.

The critical lane volume on the major road changes to 440 vehicles per hour per lane and the critical lane volume on the minor road remains unchanged. The green time will



- (A) increase for the major road and remain same for the minor road.
- (B) Increase for the major road and decrease for the minor road.
- (C) Decrease for both the roads.
- (D) Remain unchanged for both the roads.
- 64. It is proposed to widen and strengthen an existing 2-lane NH section as a divided highway. The existing traffic in one direction is 2500 commercial vehicles (CV) per day. The construction will take 1 year. The design CBR of soil subgrade is found to be 4 percent. Given: traffic growth rate for CV = 8 percent, vehicle damage factor = 3.5 (standard axles per CV), design life = 10 years and traffic distribution factor = 0.75. The cumulative standard axles (msa) computed are
  - (A) 35 (B) 37 (C) 65 (D) 70
- 65. A linear relationship is observed between speed and density on a certain section of a highway. The free flow speed is observed to be 80 km per hour and the jam density is estimated as 100 vehicles per km length. Based on the above relationship, the maximum flow expected on this section and the speed at the maximum flow will respectively be
  - (A) 8000 vehicles per hour and 80 km per hour
  - (B) 8000 vehicles per hour and 25 km per hour
  - (C) 2000 vehicles per hour and 80 km per hour
  - (D) 2000 vehicles per hour and 40 km per hour
- 66. The plan of a survey plotted to a scale of 10 m to 1 cm is reduced in such a way that a line originally 10 cm long now measures 9 cm. The area of the reduced plan is measured as 81 cm<sup>2</sup>. The actual (m<sup>2</sup>) of the survey is
  - (A) 10000 (B) 6561 (C) 1000 (D) 656

#### GATE CIVIL ENGINEERING 2008 (CE)

67. The length and bearings of a closed traverse PQRSP are given below.

Line	Length(m)	Bearing (WCB)
PQ	200	0°
QR	1000	45°
RS	907	180°
SP	?	?

The missing length and bearing, respectively of the line SP are

(A) 207 m and 270°

(B) 707 and 270°

(C) 707 m and 180°

- (D) 907 and 270°
- 68. The focal length of the object glass of a tacheometer is 200 mm, the distance between the vertical axis of the tacheometer and the optical centre of the object glass is 100 mm and the spacing between the upper and lower line of the diaphragm axis is 4 mm. With the line of collimation perfectly horizontal, the staff intercepts are 1 m (top), 2m (middle), and 3 m (bottom). The horizontal distance (m) between the staff and the instrument station is
  - (A) 100.3
- (B) 103.0
- (C) 150.0
- (D) 153.0
- 69 . A road is provided with a horizontal circular curve having deflection angle of 55° and centre line radius of 250 m. A transition curve is to be provided at each end of the circular curve of such a length that the rate of gain of radial acceleration is 0.3m/s³ at a speed of 50 km per hour. Length of the transition curve required at each of the ends is
  - (A) 2.57 m
- (B) 33.33 m
- (C) 35.73 m
- (D) 1666.67 m
- 70. A light house of 120 m height is just visible above the horizon from a ship. The correct distance (m) between the ship and the light house considering combined correction for curvature and refraction, is
  - (A) 39.098
- (B) 42.226
- (C) 39098
- (D) 42226

#### **COMMON DATA QUESTIONS**

#### Common Data for Questions 71,72 and 73:

A rectangular channel 6.0 m wide carries a discharge of 16.0m³/s under uniform condition with normal depth of 1.60 m. Manning's n is 0.015.

- 71. The longitudinal slope of the channel is
  - (A) 0.000585
- (B) 0.000485
- (C) 0.000385
- (D) 0.000285
- 72. A hump is to be provided on the channel bed. The maximum height of the jump without affecting the upstream flow condition is
  - (A) 0.50 m
- (B) 0.40 m
- (C) 0.30 m
- (D) 0.20 m
- 73. The channel width is to be contracted. The minimum width to which the channel can be contracted without affecting the upstream flow condition is
  - (A) 3.0 m
- (B) 3.8 m
- (C) 4.1 m
- (D) 4.5 m

#### GATE CIVIL ENGINEERING 2008 (CE)

#### Common Data for Questions 74 and 75:

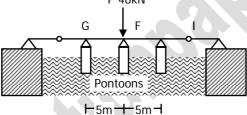
A reinforced concrete beam of rectangular cross section of breadth 230 mm and effective depth 400 mm is subjected to a maximum factored shear force of 120 kN. The grade of concrete, mains steel and stirrup steel are M20, F415 and Feb 250 respectively. For the area of main steel provided, the design shear strength  $\tau_c$  as per IS: 456-2000 is 0.48N/mm<sup>2</sup>. The beam is designed for collapse limit state.

- 74. The spacing (mm) of 2-legged 8 mm stirrups to be provided is
  - (A) 40
- (B) 115
- (C) 250
- (D) 400
- 75. In addition, the beam is subjected to a torque whose factored value is 10.90 kNm. The stirrups have to be provided to carry a shear (kN) equal to
  - (A) 50.42
- (B) 130.56
- (C) 151.67
- (D) 200.23

#### Linked Answer Questions: 76 to 85 carry two marks each

#### Statement for Linked Answer Questions 76 and 77:

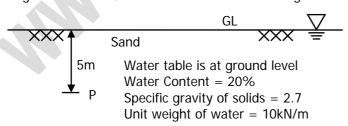
Beam GHI is supported by three pontoons as shown in the figure below. The horizontal cross-sectional area of each pontoon is 8 m<sup>2</sup>, the flexural rigidity of the beam is 10000 kN-m<sup>2</sup> and the unit weight of water is 10  $kN/m^3$ . P 48kN



- When the middle pontoon is removed, the deflection at H will be 76
  - (A) 0.2m
- (B) 0.4m
- (C) 0.6m
- (D) 0.8m
- 77 When the middle pontoon is brought back to its position as shown in the figure above, the reaction at H will be
  - (A) 8.6kN
- (B) 15.7kN
- (C) 19.2kN
- (D) 24.2kN

### Statement for Linked Answer Questions 78 and 79:

The ground conditions at a site are shown in the figure below

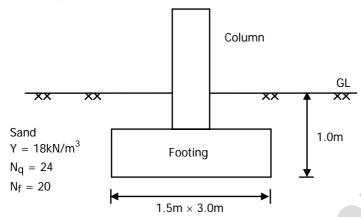


- The saturated unit weight of the sand (kN/m<sup>3</sup>) is 78.
  - (A)
- 18 (B)
- (C) 21
- (D) 24
- 79. The total stress, pore water pressure and effective stress (kN/m<sup>2</sup>) at the point P are, respectively
  - (A)
- 75, 50 and 25 (B)
- 90, 50 and 40 (C)
- 105, 50 and 55 (D)
- 120, 50 and 70

#### GATE CIVIL ENGINEERING 2008 (CE)

#### Statement for Linked Answer Questions 80 and 81:

A column is supported on a footing as shown in the figure below. The water table is at a depth of 10m below the base of the footing.



- 80. The net ultimate bearing capacity (kN/m²) of the footing based on Terzaghi's bearing capacity equation is
  - (A) 216
- (B) 432
- (C) 630
- (D) 846
- 81. The safe load (kN) that the footing can carry with a factor of safety 3 is
  - (A) 282
- (B) 648
- (C) 945
- (D) 1269

#### Statement for Linked Answer Questions 82 and 83:

An automobile with projected area  $2.6\text{m}^2$  is running on a road with speed of 120 km per hour. The mass density and the kinematic viscosity of air are  $1.2 \text{ kg/m}^3$  and  $1.5 \times 10^{-5} \text{m}^2/\text{s}$ , respectively. The drag coefficient is 0.30

- 82. The drag force on the automobile is
  - (A) 620 N
- (B) 600 N
- (C) 580 N
- (D) 520 N
- 83. The metric horse power required to overcome the drag force is
  - (A) 33.23
- (B) 31.23
- (C) 23.23
- (D) 20.23

#### Statement for Linked Answer Questions 84 and 85:

A horizontal circular curve with a centre line radius of 200 m is provided on a 2-lane, 2-way SH section. The width of the 2-lane road of 7.0 m. Design speed for this section is 80 km per hour. The brake reaction time is 2.4 s, and the coefficients of friction in longitudinal and lateral directions are 0.355 and 0.15, respectively.

- 84. The safe stopping sight distance on the section is
  - (A) 221 m
- B) 195 m
- (C) 125 m
- (D) 65 m
- 85. The set-back distance from the centre line of the inner lane is
  - (A) 7.93 m
- (B) 8.10 m
- (C) 9.60 m
- (D) 9.77 m