| DAY and TIME                                       |          | COURSE   |            | SUBJECT                   |
|--|----------|--|------------|---------------------------|
| DAY-1<br>10.30 am to 12.30 pm<br>SESSION: FORENOON | (Infrast | I.Tech/M.A<br>ructure Ma<br>ses offered<br>VCE/UBD | nagement   | ) CHEMICAL<br>ENGINEERING |
| MAXIMUM MARKS                                      | TOTAL D  | URATION  | MAXIMUM    | TIME FOR ANSWERING        |
| 100  | 150 MIN  | NUTES  |            | 120 MINUTES               |
| MENTION YOUR PO                                    | CET NO.  | JQ   | JESTION BO | OOKLET DETAILS            |
|  |          | VERSION  | CODE       | SERIAL NUMBER             |
|  |          | <b>A</b> -   | 1          | 120157                    |

### DOs:

- 1. Check whether the PGCET No. has been entered and shaded in the respective circles on the OMR answer sheet.
- 2. Ensure whether the circles corresponding to course and the specific branch have been shaded on the OMR answer sheet.
- 3. This Question Booklet is issued to you by the invigilator after the 2<sup>nd</sup> Bell i.e., after 10.25 a.m.
- 4. The Serial Number of this question booklet should be entered on the OMR answer sheet.
- 5. The Version Code of this question booklet should be entered on the OMR answer sheet and the respective circles should also be shaded completely.
- Compulsorily sign at the bottom portion of the OMR answer sheet in the space provided.

#### DON'Ts:

- 1. THE TIMING AND MARKS PRINTED ON THE OMR ANSWER SHEET SHOULD NOT BE DAMAGED/MUTILATED/SPOILED.
- 2. The 3rd Bell rings at 10.30 a.m., till then;
  - Do not remove the paper seal / polythene bag of this question booklet.
  - Do not look inside this question booklet.
    - Do not start answering on the OMR answer sheet.

### IMPORIANT INSTRUCTIONS TO CANDIDATES

- 1. This question booklet contains 75 (items) questions and each question will have one statement and four answers. (Four different options / responses.)
- 2. After the 3<sup>rd</sup> Bell is rung at 10.30 a.m., remove the paper seal / polythene bag of this question booklet and check that this booklet does not have any unprinted or torn or missing pages or items etc., if so, get it replaced by a complete test booklet. Read each item and start answering on the OMR answer sheet.
- 3. During the subsequent 120 minutes:
  - Read each question (item) carefully.
  - Choose one correct answer from out of the four available responses (options / choices) given under each question / item. In case you feel that there is more than one correct response, mark the response which you consider the best. In any case, choose only one response for each item.
  - Completely darken / shade the relevant circle with a BLUE OR BLACK INK BALL POINT PEN against the question number on the OMR answer sheet.
- 4. Use the space provided on each page of the question booklet for Rough Work. Do not use the OMR answer sheet for the same.
- 5. After the last Bell is rung at 12.30 pm, stop marking on the OMR answer sheet and affix your left hand thumb impression on the OMR answer sheet as per the instructions.
- 6. Hand over the OMR ANSWER SHEET to the room invigilator as it is.
- 7. After separating the top sheet, the invigilator will return the bottom sheet replica (Candidate's copy) to you to carry home for self-evaluation.
- 8. Preserve the replica of the OMR answer sheet for a minimum period of ONE year.
- Only Non-programmable calculators are allowed.

### **Marks Distribution**

PART-I : 50 QUESTIONS CARRY ONE MARK EACH (1 TO 50) PART-II : 25 QUESTIONS CARRY TWO MARKS EACH (51 TO 75)

003-A1

A-1 2

## CHEMICAL ENGINEERING PART – I

# Each question carries one mark.

 $(50\times1=50)$ 

| 1. | In a given system, extensive property of | f a thermodynamic system depends u | pon |
|----|--|------------------------------------|-----|
|    | · · · · · ·                              | •                                  |     |

- (A) Pressure & temperature
- (B) Viscosity

(C) Mass

(D) Volume

2. Enthalpy for the reaction 
$$C + O_2 \rightarrow CO_2$$
 is

(A) Positive

(B) Negative

(C) Zero

(D) None of these

(A)  $\left(\frac{\partial E}{\partial T}\right)_{P}$ 

(B)  $\left(\frac{\partial H}{\partial H}\right)_{B}$ 

(C)  $\left(\frac{\partial S}{\partial T}\right)_{P}$ 

(D) None of these

# 4. Joule - Thomson coefficient for a perfect gas is

(A) Zero

(B) Positive

(C) Negative

(D) None of these

# 5. For a chemical reaction occurring at equilibrium under constant temperature and pressure, the change in Gibbs free energy is

(A) Maximum

(B) Minimum

(C) Zero

(D) None of these

| 6   | The<br>CaC | number of degrees CO <sub>3</sub> into an evacuated s | of freedom for space is     | a system prepared by partially decomposing |
|-----|------------|---|-----------------------------|--|
|     | (A)        | 0   | er to say the Commission (B |  |
|     | (C)        | 2   |                             | ) 3<br>- 1                                 |
| 7.  | A ro       | tameter is a device use                               | ed to measure               |  |
|     | (A)        | Velocity of fluid in p                                |                             |  |
|     | (C)        | Vortex flow   | (D                          | -  |
| 8.  | Cavit      | ation is caused by                                    | ;                           | en e   |
|     | (A)        | High velocity   | <b>(B</b> )                 | Low Barometric pressure                    |
|     | (C)        | High pressure   | ( <b>D</b> )                |  |
| 9.  | For m      | easuring flow by a Ve                                 | nturimeter, it sho          | ould be installed in                       |
|     | (A)        | Vertical line   | ( <b>B</b> )                |  |
| • , | (C)        | Horizontal line                                       | (D)                         |  |
| 10. | A larg     | e Reynold's number is                                 | s indication of             |  |
|     |            | Laminar flow  | <b>(B)</b>                  | Steady flow                                |
|     | (C) S      | Smooth and stream line                                |                             | Highly turbulent flow                      |
| 11. | Mesh i     | s defined as the number                               |                             |  |
|     | (A) Fe     | et of screen surface                                  | ( <b>B</b> )                | Inch of screen surface                     |
|     |            | eter of screen surface                                | (D)                         | None of these                              |
| 12. | Specifi    | c surface of spherical t                              | particles is given          | by - Marian Araban Araban Araban           |
|     | (A) 6      | / Dp  | (B)                         | 2/Dρ                                       |
|     | (C) 4      | / Dρ  | •                           | 12 / Dp                                    |

| 12  | For non – spherical particle, the sphericity (φ) is defined by the relation   |
|-----|---|
| 13. | $(B)  \phi_s = (D_p S_p) / V_p$   |
|     | (A) $\phi_S = V_P / (D_P S_P)$<br>(C) $\phi_S = 6V_P / (D_P S_P)$<br>(D) $\phi_S = V_P / (6D_P S_P)$  |
| 14. | Ball mill is used for  (A) Crushing (C) Fine grinding  (B) Coarse grinding (D) Attrition  |
| 15. | The unit of specific cake resistance is   |
|     | (A) $kg/m^2$ (B) $m/kg$ (C) $m/kg^2$ (D) $kg/m^3$   |
| 16. | Dropwise condensation usually occurs on  (A) Glazed surface  (B) Smooth surface  (C) Oil surface  (D) Coated surface  |
| 17  | least in  (A) Parallel flow  (C) Cross flow  (B) Counter flow  (D) Same iff all above   |
| 18  | (A) an insulator (B) conductor and insulator (C) a super conductor (D) a fin  |
| 1   | P. Emissivity of a body is equal to absorptivity if the body is  (A) in thermal equilibrium  (B) at low temperature  (C) at high temperature  (D) none of these |

| 2                                 | 20. A ra                  | adiation shield should have   |                        |   |
|-----------------------------------|---------------------------|---|------------------------|---|
|                                   | (A)                       |   | (1                     | B) Low reflectivity   |
|                                   | (C)                       | High reflectivity   | •                      | D) None of these  |
| 2                                 | 1. The                    | effect of scaling in a heat exchange  | anger is               |   |
|                                   | (A)<br>(C)                | Heat transfer coefficient Insulation factors  | (E                     | B) Fouling factors  |
| 22                                | ()                        | transfer coefficient (K) and dis $K \propto D$ $K \propto D^{1.5}$  | <b>(B</b> )            | $K(D)$ are related according to film theory is $K \propto \sqrt{D}$ $K \propto D^2$   |
| 23.                               | (A)                       | inary diffusivity in gases deper<br>Temperature<br>Nature of components   | nds upor<br>(B)<br>(D) | Pressure  |
| <ul><li>24.</li><li>25.</li></ul> | (A) I (C) I Ratio c (A) H | t's law is applicable to Ideal solutions Mixture of water and alcohol of the partial pressure of the var Iumidity Relative humidity | (B)                    | Real solutions All of these he vapour pressure of liquid is called Saturated humidity |
| 26.                               | Cox cha                   | art is used in the design of istillation column eat exchanger   | (D) (B) (D)            | None of these  Condensor  Crystallizer  |

| 27. | The | rate | of | leaching | depends | or |
|-----|-----|------|----|----------|---------|----|
|-----|-----|------|----|----------|---------|----|

(A) The particle size

(B) The temperature

(C) The agitation

(D) All of these

## 28. Schmidt number (N<sub>SC</sub>) is defined as

(A)  $\mu/D_{AB}$ 

(B)  $\mu / \rho D_{AB}$ 

(C)  $\rho\mu/D_{AB}$ 

(D)  $\mu D_{AB} / \rho$ 

# 29. Ficks second law of diffusion in one dimension is

- (A)  $\partial C_A / \partial t = D_{AB} (\partial^2 C_A) / (\partial x^2)$
- (B)  $\partial C_A / \partial t = D_{AB} (\partial C_A) / (\partial x)$

(C)  $\partial C_A / \partial t = (\partial C_A) / (\partial x)$ 

(D) None of these

# 30. The rate of chemical reaction depends upon

(A) Temperature

(B) Pressure

(C) Concentration

(D) All of these

# 31. Space time in flow reactor is

- (A) Usually equal to the residence time
- (B) The reciprocal of the space velocity
- (C) Both (A) and (B)
- (D) None of these

# 32. BET apparatus is used to determine

- (A) Specific surface of porous catalyst
- (B) Pure size distribution
- (C) Pore diameter
- (D) Porosity of the catalyst bed

- 33. What is the dispersion number for a CSTR?
  - (A) 0

**B**) 1

(C) < 1

- (D) ∞
- 34. Which of the following explains the mechanism of catalysis?
  - (A) Activated complex theory
- (B) Collosion theory

1-15-25

- (C) Thermodynamics
- (D) None of these
- 35. Those material which improves the activity of a catalyst is called
  - (A) Carrier

(B) Promoter

(C) Inhibitor

- (D) None of these
- 36. If E is the age distribution of fluid leaving a vessel, then

(A) 
$$\int_{0}^{\infty} E.dt = 0$$

$$\lim_{A \to \infty} e^{tx} \qquad \lim_{A \to \infty} (B) \qquad \int_{0}^{\infty} E.dt = 1$$

(C) 
$$\int_{0}^{\infty} E.dt = \infty$$

(D) 
$$\int_{0}^{\infty} E.dt = \frac{2}{\pi}$$

- 37. Characterization of a dynamic system by a transfer function can be done for
  - (A) Linear system

(B) Non – linear system

(C) Both (A) & (B)

- (D) None of these
- 38. Phase angle  $(\phi)$  of the sinsusoidal response of first order system is given by
  - (A)  $\phi = \tan h^{-1} (\omega \tau)$

(B)  $\phi = \tan^{-1}(-\omega\tau)$ 

(C)  $\phi = \tan^{-1}(\omega \tau)$ 

(D)  $\phi = \tan h^{-1} (-\omega \tau)$ 

| 39. | With a damping coefficient m  | ore than 1 the se              | cond order wift be        |  |
|-----|---|--------------------------------|---------------------------|--|
| 37. | As TI In dommed   | 90 45 (B)                      | Oscillatory               | ic as  |
|     | (C) Over damped   | configuration (D)              | Critically damped         | l e e e e e e e e e e e e e e e e e e e  |
| 40. | Routh test cannot be used to  | test the stability             | of a control system       | containing   |
|     | (A) Controller  | 2 / (E).                       | 'I Tansportation la       | g Lac Services   |
|     | (C) Final control element   |                                | None of these             | Maria de la Caracteria de<br>Caracteria de la Caracteria   |
|     |   | (4) · · · 2                    |                           |  |
| 41. | Diameter of the distillation of   | column is set by               |                           |  |
|     | (A) Number of theoretical   | plates work                    | partition grading success | entre de la companya del companya de la companya del companya de la companya de   |
|     | (B) Allowable vapour ven  | City                           |                           |  |
|     |   | and the control of             |                           |  |
|     | <ul><li>(C) Static submergence</li><li>(D) Length of straight rec</li></ul> | tangular weir on               | cross flow tray           |  |
| 42. | (A) 0 (C) > 1   | (B<br>81024 (E<br>25(m) ) 3    | )                         | ion column is weak, the second water   |
|     | Break – even point is the r   | •                              |                           |  |
| 43  | (A) Unit price  |                                | 12.5 - 10.00 1 1          | and the second section of the section o |
|     | (B) Unit variable cost  |                                | 2.4<br>2.4                |  |
|     | (C) Unit price + Unit va  |                                | 3                         |  |
|     | (D) Unit price – Unit va  | riable cost                    |                           |  |
| 4   | 4. Sucrose content in cane s  | ોલ મુગ્યું<br>ugar may be aroi | ind                       | Same of the second seco |
| 7   | (A) 30%   | Ano ment                       | (B) 70%                   |  |
|     | (C) 80%   | and it                         | (D) 95%                   |  |
|     |   | Space For                      | Rough Work                |  |

| 4   | <b>5.</b> U | Iltimate              | analysis of coal o                     | letermines                         |                |  |
|-----|-------------|-----------------------|--|------------------------------------|----------------|--|
|     |             | A) Carl               |  |                                    | B)             | Hydrogen   |
|     | (0          | C) Sulp               | ohur                                   |                                    | D)             |  |
| 40  | 6. A        | solution<br>specific  | of specific grave<br>c gravity of A is | ity 1.0 consists 0.7, the specific | of             | 35% A by weight and the remaining 'B' if             |
|     | (A          | ) 1.25                |  |                                    |                | 1.3  |
|     | (C)         | 1.35                  |  | (I                                 | ))             | 1.2  |
| 47  | . For       | r the cas<br>adiabati | e of fuel gas und<br>ic flame tempera  | lergoing combu                     | sti            | on with air, if the air/fuel ratio is increased,     |
|     | (A)         | Increa                | ases                                   | <b>(B</b>                          | )              | Decreases  |
|     | (C)         | Deper                 | nds on fuel type                       |                                    | -              | None of these  |
| 48. | An<br>com   | aqueous               | s solution of 2.4.                     | 5% by weight   rmality is          | H <sub>2</sub> | SO <sub>4</sub> has a specific gravity of 1.011. The |
|     | (A)         | 0.25                  |  | <b>(B</b> )                        | k.             | 0.2528   |
|     | (C)         | 0.5                   |  | (D)                                |                | 0.5055   |
| 49. | Knuc        | dson dif              | fusion is directly                     | proportional to                    |                |  |
|     | (A)         | T                     |  | <b>(B)</b>                         |                | $\sqrt{	ext{T}}$                                     |
|     | (C)         | 1∕√T                  |  | (D)                                | ,              | <b>[2</b> ]  |
| 50. | Rate        | of autoc              | atalytic chemical                      | reaction is a fu                   | nc             | tion of  |
|     | (A)         |                       | ature only                             | (B)                                |                | ressure only   |
|     | (C)         |                       | sition only                            | (D)                                |                | all of these   |
|     |             |                       |  | Space For Rou                      | gh             | Work   |

51. The change in free energy when a real gas undergoes an isothermal change in state is

- (A)  $\Delta G = RT \ln (V_2/V_1)$
- (B)  $\Delta G = RT \ln (P_2/P_1)$

- (C)  $\Delta G = RT \ln (f_2/f_1)$
- (D)  $\Delta G = RT \ln (\gamma_2/\gamma_1)$

52. The equilibrium constant for the reaction  $N_2 + 3H_2 \rightarrow 2$  NH<sub>3</sub> is 0.1084. Under the same conditions, the equilibrium constant for the reaction 1/2 N<sub>2</sub> + 3/2 H<sub>2</sub>  $\leftrightarrow$  NH<sub>3</sub> is

(A) 0.1084

(B) 0.3292

(C) 0.0118

(D) 0.0542

53. What is the change in entropy when 1 gm of ice at 0°C is converted to steam at 100°C?  $C_p$  of water is 1 cal/g,  $\lambda_{vap} = 540$  cal/g

(A) 0.553 cal/g K

(B) 1.053 cal/g K

(C) 2.053 cal/g K

(D) None of these

54. Critical speed of ball mill is equal to

(A) 1/(D-d)

(B)  $1/\sqrt{D-d}$ 

(C)  $76.65 / \sqrt{D-d}$ 

(D)  $76.75 / \sqrt{D-d}$ 

55. Percentage of drum submerged in slurry in case of rotary drum filter is

(A) 3

**(B)** 30

(C) 85

(D) None of these

| 50         | 6. A | s<br>roj   | teel ball of mass pped into 1 kg wa                   | 1 kg and specter at 20 °C.                | cific hea<br>The fina    | t 0.4 k<br>l steady          | J/kg is<br>y state t        | at a ter<br>tempera         | nperatur      | e of 60 vater is       | °C. It is |
|------------|------|------------|---|---|--------------------------|------------------------------|-----------------------------|-----------------------------|---------------|------------------------|-----------|
|            |      |            | 23.5 °C   |   | (E                       |                              |                             |                             |               |                        |           |
|            | ((   | <b>C</b> ) | 35 °C   |   | (E                       | 9) 40                        | °C                          |                             | • *           |                        |           |
| 57.        |      | or<br>ssi  | a current wire of pation occurs who                   | 20 mm diam<br>en thickness o              | eter export              | osed to<br>ion (K            | o air (h<br>= 0.5 V         | = 20 V<br>V/mK)             | V/m² K)<br>is | , maxim                | um heat   |
|            | (A   | .)         | 20 mm   |   | <b>(B</b> )              | 25 1                         | mm                          |                             |               |                        |           |
|            | (C   | )          | 35 mm   |   | <b>(D</b> )              | 10 r                         | mm                          |                             |               |                        |           |
|            |      |            |   |   |                          |                              |                             |                             |               |                        |           |
| 58.        | 26   | °C         | certain heat exchange. The hot fluid leaves at 55 °C. | anger, both the distance of the effective | e fluids °C and eness of | have ic<br>leaves<br>heat ex | dentical<br>at 47<br>change | l mass i<br>°C and<br>er is | low rat       | e – speci<br>d fluid e | fic heat  |
|            | (A)  | )          | 0.16  |   | <b>(B)</b>               | 0.58                         |                             |                             |               |                        |           |
|            | (C)  |            | 0.72  |   | (D)                      | 1.0                          |                             |                             |               | z                      |           |
|            |      |            |   |   |                          |                              |                             |                             |               |                        |           |
| <b>59.</b> | NT   | U i        | is calculated by th                                   | e equation                                |                          |                              |                             |                             |               |                        |           |
|            | (A)  | 1          | UA/C <sub>min</sub>                                   |   | (B)                      | UA (                         | C <sub>min</sub>            |                             | . 4           |                        |           |
|            | (C)  | •          | C <sub>min</sub> / UA                                 |   | (D)                      | C <sub>min</sub>             | / C <sub>max</sub>          | •                           |               |                        |           |
| 60.        | Four | rie        | r's law of heat co                                    | nduction give                             | s the hea                | t flow:                      | for                         |                             |               |                        | *         |
|            | (A)  | C          | One dimensional f                                     | low only                                  | <b>(B)</b>               | Two                          | dimensi                     | ional flo                   | w only        |                        |           |
|            | (C)  | I          | rregular surfaces                                     | only                                      | (D)                      | All su                       |                             |                             | <b>-</b>      |                        |           |
|            |      |            | <del></del>   | Space 1                                   | For Rou                  | gh Wor                       | rk                          |                             |               |                        |           |
|            |      |            |   |   |                          |                              |                             |                             |               |                        |           |

|     | (A)        | listilla<br>0.5 d             | & 0.75             |            |            |       |        | (B)           | 0.25 & 0.5                       |                                |
|-----|------------|-------------------------------|--------------------|------------|------------|-------|--------|---------------|----------------------------------|--------------------------------|
|     | • .        |                               | <b>&amp;</b> 0.9   |            |            |       | -      | (D)           | 0.75 & 0.75                      |                                |
| 62. | Matc       | h list                        | I with             | list II    | and s      | elect | the co | orrect a      | nswer from the                   | codes given below the lists:   |
|     |            |                               | LIS                | T – I      |            | i (j) |        |               | LIST – II                        |                                |
|     | (a)        | Rota                          | ary ato            | mizer      |            |       |        | (1)           | Kinetic energy                   |                                |
|     | (b)        | Rela                          | ative v            | olatilit   | y          |       |        | (2)           | Centrifugal pur                  | mp                             |
|     | (c)        | Pne                           | umatic             | nozzl      | e          |       |        | (3)           | Distillation                     |                                |
|     | (d)        | Sele                          | ectivity           | 7          |            |       |        | (4)           | Liquid - liquid                  | l extraction                   |
|     |            | (a)                           | (b)                | (c)        | ' (d)      |       |        |               |                                  |                                |
|     | (A)        | 2                             | 3                  | 1          | 4          |       |        |               |                                  |                                |
|     | <b>(B)</b> | 2                             | -1                 | <b>3</b> . | 4          |       |        |               |                                  |                                |
|     | (C)        | 1                             | 2                  | 3          | 4          |       |        |               |                                  |                                |
|     | (D)        | 4                             | 3                  | 1          | 2          |       |        |               |                                  |                                |
|     |            |                               |                    |            |            | _     |        | * .           |                                  | t at a standard management     |
| 63. | Acc<br>to  | ordin                         | g to si            | ırface ·   | – ren      | ewal  | theor  | y, mas        | s transier coeiiic               | cient is directly proportional |
|     | (A)        | $\mathbf{D}_{\mathbf{A}^{1}}$ | В                  |            |            |       |        | <b>(B)</b>    | $D^2_{AB}$                       | 2*                             |
|     | (C)        | $\mathbf{D}^{1.}$             | 5<br>AB            |            | * :<br>* : |       |        | (D)           | $\mathbf{D^{0.5}}_{\mathbf{AB}}$ |                                |
| 64. | The        | psyc                          | homet              | ric rati   | o is d     | efine | d as   | 41.1<br>4.11. |                                  |                                |
|     | (A)        | $\mathbf{h}_{\mathbf{G}}$     | / Ky               |            |            |       |        | <b>(B)</b>    | $K_y / h_G$                      |                                |
|     | (C)        | hc                            | / K <sub>y</sub> C | · · · ·    |            |       |        | (D)           | $N_{SC}/N_{pr}$                  |                                |

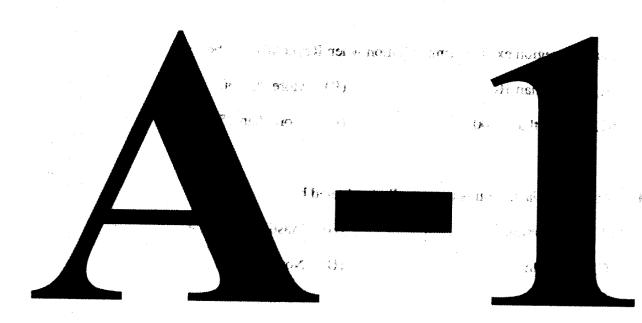
| 65.        | Rota              | ary driers are operated with the hole  | dups c            | of material in the range of  |
|------------|-------------------|--|-------------------|--|
|            | (A)               | 0.20 to 0.30   | <b>(B)</b>        |  |
|            | (C)               | 0.40 to 0.50   | (D)               | 0.05 to 0.15   |
| 66.        | If r <sub>A</sub> | $c = - d C_A / dt = 0.2 \text{ mol/lit-sec whe}$<br>= 10 mol / lit ?   | en C <sub>A</sub> | = 1 mol/lit, what is the rate of reaction when   |
|            | (A)               | 2 mol/lit.sec  | (B)               | 0.2 mol (lit.sec)  |
|            |                   | 20 mol/sec   |                   | 0.02 mol/lit.sec   |
| 67.        |                   | rate equation for an autocatalytic re  |                   |  |
|            | <b>A</b> + 3      | $R \xrightarrow{k_1} R + R \text{ is } -r_A = d C_A/dt = R$  | C CA C            | C <sub>R</sub> plot of (-r <sub>A</sub> ) versus C <sub>A</sub> gives a  |
|            | (A)               |  | <b>(B)</b>        | Parabola   |
|            | (C)               | Hyperbola  | (D)               | Straight line with zero slope  |
| 68.        | of co<br>with     | on irreversible elementary first order<br>concentration of component R versus slope of $\mathbf{k}_1 + \mathbf{k}_2$ | s conc            | tion in parallel A $\xrightarrow{k_1}$ R; A $\xrightarrow{k_2}$ S. A plot centration of components gives a straight line |
|            |                   |  |                   | $\mathbf{k}_1 - \mathbf{k}_2$  |
|            | (C)               | <b>k</b> <sub>2</sub> / <b>k</b> <sub>1</sub>  | (D)               | $k_1/k_2$  |
| 69.        | The t             | ransfer function of a PD controller  | is                |  |
|            | (A)               | $K_C / \tau_D S$   | <b>(B)</b>        | $K_{C}(1+1/\tau_{D}S)$   |
|            | (C) I             | $K_{C} (1 + \tau_{D}S)$  | (D)               | $K_{\rm C} (1 + \tau_{\rm D}/S)$   |
| <b>70.</b> | At the            | e corner frequency, amplitude rati   | io (AF            | R) for the sinusoidal response of first order  |
|            | (A)               | $1/\sqrt{2}$   | <b>(B)</b>        | b  |
|            | (C)               | $\sqrt{2}$   | (D)               | 1√5  |
|            |                   | Space Fo   | r Rou             | gh Work  |
| •          |                   |  |                   |  |

|            | ` '        | Over shoot = decay ratio                 | <b>(B)</b> | Over shoot = $(\text{decay ratio})^2$ |
|------------|------------|--|------------|---------------------------------------|
|            | (C) (      | Over shoot = $\sqrt{\text{decay ratio}}$ | (D)        | Over shoot = $(\text{decay ratio})^3$ |
| 72.        | Accu       | racy is specified as ± 0.5% of tru       | ie value.  | At 5% of full scale, error of the     |
|            | instru     | ıment will be                            |            |                                       |
|            | (A)        | (±) 0.025%                               | (B)        | (±) 0.5%                              |
|            | (C)        | (±) 2.5%                                 | <b>(D)</b> | (±) 25%                               |
|            |            |  |            |                                       |
| <b>73.</b> | Lam        | inar region exists during agitation      | n when F   | Reynold's number is                   |
|            | (A)        | Less than 10                             | <b>(B)</b> | More than 50                          |
|            | (C)        | More than 1000                           | <b>(D)</b> | More than 2500.                       |
|            |            | 1<br>- 18                                |            |                                       |
| 74.        | Mix        | ing of plastic solids is generally i     | incilitate | d by                                  |
|            | (A)        | Dispersion                               | <b>(B)</b> | Mastication .                         |
|            | (C)        | Kneading                                 | (D)        | Nome of these                         |
|            |            |  |            |                                       |
| 75.        | Poly       | rtetrafluroethylene (PTFE) is kno        | wn as      |                                       |
|            | <b>(A)</b> | Teflon                                   | <b>(B)</b> | Decron                                |
|            | (C)        | Perspex                                  | (D)        | Nylon                                 |
|            |            | · -                                      |            | ugh Work                              |

71. In under damped second – order response

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