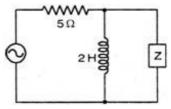


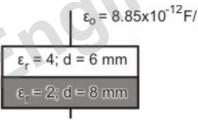
## **Electrical Engineering - 2004**

## **Full Paper**

1. The value of Z in Figure which is most appropriate to cause parallel resonance at 500 Hz is



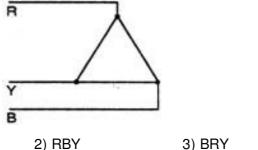
- 1) 125.00 mH
- 2) 304.20 µF
- 3)  $2.0 \mu F$
- 4)  $0.05 \mu F$
- 2. A parallel plate capacitor is shown in Figure. It is made of two square metal plates of 400 mm side. The 14 mm space between the plates is filled with two layers of dielectrics of  $\epsilon_r$  = 4, 6 mm thick and  $_r$  = 2, 8 mm thick. Neglecting fringing of fields at the edges the capacitance is



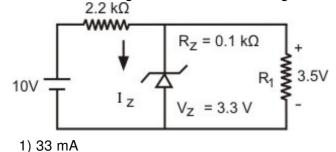
- 1) 1298 pF
- 2) 944 pF
- 3) 354 pF
- 4) 257 pF
- 3. The inductance of a long solenoid of length 1000 mm wound uniformly with 3000 turns on a cylindrical paper tube of 60 mm diameter is
  - 1) 3.2 μH
  - 2) 3.2 mH
  - 3) 32.0 mH
  - 4) 3.2 H
- 4. Total instantaneous power supplied by a 3-phase ac supply to a balanced R-L load is
  - 1) zero
  - 2) constant
  - 3) pulsating with zero average

- pulsating with non-zero average
- 5. A 500 kVA, 3-phase transformer has iron losses of 300 W and full load copper losses of 600 W. The percentage load at which the transformer is expected to have maximum efficiency is
  - 1) 50.0%
  - 2) 70.7%
  - 3) 141.4%
  - 4) 200.0%
- 6. For a given stepper motor, the following torque has the highest numerical value.
  - 1) Detent torque
  - 2) Pull-in torque
  - 3) Pull-out torque
  - 4) Holding torque
- eers.com 7. The following motor definitely has a permanent magnet rotor
  - 1) DC commutator motor
  - 2) Brushless dc motor
  - 3) Stepper motor
  - 4) Reluctance motor
- 8. The type of single-phase induction motor having the highest power factor at full load is
  - 1) shaded pole type
  - 2) split-phase type
  - 3) capacitor-start type
  - 4) capacitor-run type
- 9. The direction of rotation of a 3-phase induction motor is clockwise when it is supplied with 3-phase sinusoidal voltage having phase sequence A-B-C. For counterclockwise rotation of the motor, the phase sequence of the power supply should be
  - 1) B-C-A
  - 2) C-A-B
  - 3) A-C-B
  - 4) B-C-A or C-A-B
- 10. For a linear electromagnetic circuit, the following statement is true.
  - 1) Field energy is equal to the co-energy
  - 2) Field energy is greater than the co-energy
  - 3) Field energy is lesser than the co-energy
  - 4) Co-energy is zero
- 11. The rated voltage of a 3-phase power system is given as

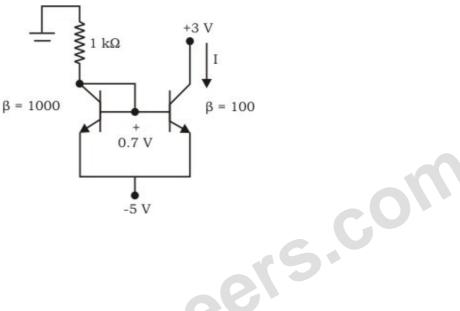
- 1) rms phase voltage
- 2) peak phase voltage
- 3) rms line to line voltage
- 4) peak line to line voltage
- 12. The phase sequence of the 3-phase system shown in Figure is



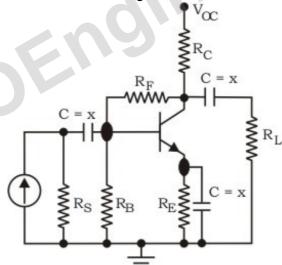
- 1) RYB
- 3) BRY
- 4) YBR
- 13. In thermal power plants, the pressure in the working fluid cycle is developed by
  - 1) condenser
  - 2) super heater
  - 3) feed water pump
  - 4) turbine
- 14. For harnessing low variable waterheads, the suitable hydraulic turbine with high percentage of reaction and runner adjustable vanes is
  - 1) Kaplan
  - 2) Francis
  - 3) Pelton
  - 4) Impeller
- 15. The transmission line distance protection relay having the property of being inherently directional is
  - 1) impedance relay
  - 2) MHO relay
  - 3) OHM relay
  - 4) reactance relay
- 16. The current through the Zener diode in Figure is



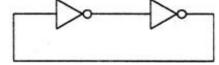
- 2) 3.3 mA
- 3) 2 mA
- 4) 0 mA
- 17. Two perfectly matched silicon transistors are connected as shown in Figure. The value of the current I is



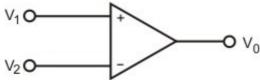
- 1) 0 mA
- 2) 2.3 mA
- 3) 4.3 mA
- 4) 7.3 mA
- 18. The feedback used in the circuit shown in Figure, can be classified as



- 1) shunt-series feedback
- 2) shunt-shunt feedback
- 3) series-shunt feedback
- 4) series-series feedback
- 19. The digital circuit using two inverters shown in Figure will act as

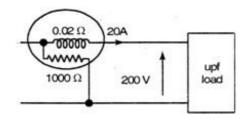


- 1) a bistable multi-vibrator
- 2) an astable multi-vibrator
- 3) a monostable multi-vibrator
- 4) an oscillator
- 20. The voltage comparator shown in Figure, can be used in the analog-to-digital conversion as

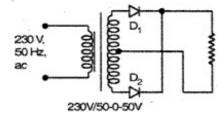


- 1) a 1-bit quantizer
- 2) a 2-bit quantizer
- 3) a 4-bit quantizer
- 4) a 8-bit quantizer
- 21. The Nyquist plot of loop transfer function G(s) H(s) of a closed loop control system passes through the point (-1, j0) in the G(s) H(s) plane. The phase margin of the system is
  - 1) 0°
- 2) 45°
- 3) 90°
- 4) 180°
- 22. Consider the function,  $F(s) = 5/(s(s^2 + 3s + 2))$  where F(s) is the Laplace transform of the function f(t). The initial value of f(t) is equal to
  - 1) 5

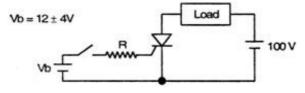
- 2) 5/2
- 3) 5/3
- 4) 0
- 23. For a tachometer, if  $\theta(t)$  is the rotor displacement is radians, e(t) is the output voltage and  $K_t$  is the tachometer constant in V/rad/sec, then the transfer function, E(s)/Q(s) will be
  - 1)  $K_t s^2$
  - 2) K<sub>t</sub>/s
  - 3) K<sub>t</sub>s
  - 4) K<sub>1</sub>
- 24. A dc potentiometer is designed to measure up to about 2 V with a slide wire of 800 mm. A standard cell of emf 1.18 V obtains balance at 600 mm. A test cell is seen to obtain balance at 680 mm. The emf of the test cell is
  - 1) 1.00 V
  - 2) 1.34 V
  - 3) 1.50 V
  - 4) 1.70 V
- 25. The circuit in Figure, is used to measure the power consumed by the load. The current coil and the voltage coil of the wattmeter have  $0.0\mathbf{\Omega}$  and  $1000\Omega$  resistances respectively. The measured power compared to the load power will be



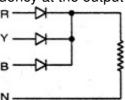
- 1) 0.4% less
- 2) 0.2% less
- 3) 0.2% more
- 4) 0.4% more
- 26. A galvanometer with a full scale current of 10 mA has a resistance of  $\Omega.100$  multiplying power (the ratio of measured current to galvanometer current) of a  $\Omega.100$  shunt with this galvanometer is
  - 1) 110
- 2) 100
- 3) 11
- 4) 10
- 27. A bipolar junction transistor (BJT) is used as a power control switch by biasing it in the cutoff region (OFF state) or in the saturation region (ON state). In the ON state, for the BJT
  - 1) both the base-emitter and base-collector junctions are reverse biased
  - 2) the base-emitter junction is reverse biased, and the base-collector junction is forward biased
  - 3) the base-emitter junction is forward biased, and the base-collector junction is reverse biased
  - 4) both the ,base-emitter and base-collector junctions are forward biased
- 28. The circuit in Figure shows a full-wave rectifier. The input voltage is 230 V (rms) single-phase ac. The peak reverse voltage across the diodes  $D_1$  and  $D_2$  is



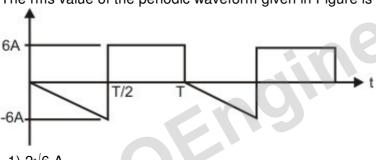
- 1) 100 √2 V
- 2) 100 V
- 3) 50 √2 V
- 4) 50 V
- 29. The triggering circuit of a thyristor is shown in Figure. The thyristor requires a gate current of 10 mA, for guaranteed turn-on. The value of R required for the thyristor to turn on reliably under all conditions of Vb variation is



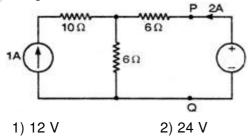
- 1)  $10000 \Omega$
- 2)  $1600 \Omega$
- 3)  $1200 \Omega$
- 4) 800 Ω
- 30. The circuit in Figure shows a 3-phase half-wave rectifier. The source is a symmetrical, 3phase four-wire system. The line-to-line voltage of the source is 100 V. The supply frequency is 400 Hz. The ripple frequency at the output is



- 1) 400 Hz
- 2) 800 Hz
- 3) 1200 Hz
- 4) 2400 Hz
- 31. The rms value of the periodic waveform given in Figure is



- 1) 2√6 A
- 2) 6√2 A
- 3) √(4/3) A
- 4) 1.5 A
- 32. In Figure, the value of the source voltage is

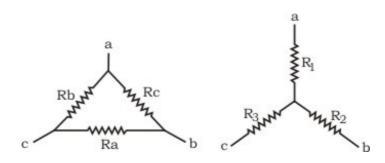


3) 30 V

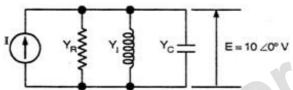
4) 44 V

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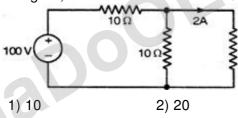
33. In Figure, Ra, Rb and Rc are 20  $\Omega$ , 10  $\Omega$  respectively. The resistances R1, R2 and R3 in  $\Omega$ of an equivalent star-connection are



- 1) 2.5, 5, 5
- 2) 5, 2.5, 5
- 3) 5, 5, 2.5
- 4) 2.5, 5, 2.5
- 34. In Figure, the admittance values of the elements in Siemens are  $Y_R = 0.5 + j0$ ,  $Y_1 = 0 j1.5$ ,  $Y_C = 0 + j0.3$  respectively. The value of I as a phasor when the voltage E across the elements is  $10|0^{\circ}$  V is



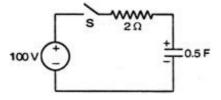
- 1) 1.5 + j0.5
- 2) 5 j18
- 3) 0.5 + j1.8
- 4) 5 j12
- 35. In Figure, the value of resistance R in  $\Omega$  is



3) 30

4) 40

36. In Figure, the capacitor initially has a charge of 10 Coulomb. The current in the circuit one second after the switch S is closed will be



- 1) 14.7 A
- 2) 18.5 A
- 3) 40.0 A
- 4) 50.0 A
- 37. The rms value of the resultant current in a wire which carries a dc current of 10 A and a

sinusoidal alternating current of peak value 20 A is

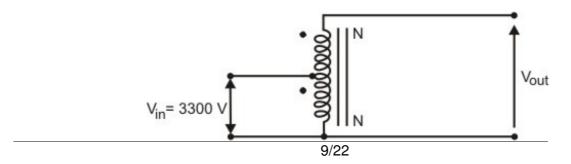
- 1) 14.1 A
- 2) 17.3 A
- 3) 22.4 A
- 4) 30.0 A
- 38. The Z matrix of a 2-port network as given by
  - 0.9 0.2

The element Y22 of the corresponding Y matrix of the same network is given by

- 1) 1.2
- 2) 0.4
- 3) -0.4
- 4) 1.8

5.CO

- 39. The synchronous speed for the seventh space harmonic mmf wave of a 3-phase, 8 pole, 50 Hz induction machine is
  - 1) 107.14 rpm in forward direction
  - 2) 107.14 rpm in reverse direction
  - 3) 5250 rpm in forward direction
  - 4) 5250 rpm in reverse direction
- 40. A rotating electrical machine having its self-inductances of both the stator and the rotor windings, independent of the rotor position will be definitely not develop
  - 1) starting torque
  - 2) synchronizing torque
  - 3) hysteresis torque
  - 4) reluctance torque
- 41. The armature resistance of a permanent magnet dc motor is 0.8Ω. At no load, the motor draws 1.5 A from a supply voltage of 25 V and runs at 1500 rpm. The efficiency of the motor while it is operating on load at 1500 rpm drawing a current of 3.5 A from the same source will be
  - 1) 48.0%
  - 2) 57.1%
  - 3) 59.2%
  - 4) 88.8%
- 42. A 50 kVA, 3300/230 V single-phase transformer is connected as an autotransformer shown in Figure. The nominal rating of the autotransformer will be



	nase, 230 V, 50 Hz, 4 pol mpedances	e, capacitor-start ind	uction motor has the following
	$rac{1}{2}$ ng $Z_m = 6.0 + j4.0 Ω$		60
	inding $Z_a = 8.0 + j6.0 \Omega$		
	of the starting capacitor red the main and auxiliary wind	•	phase difference between the
1) 176.84	μF		
2) 187.24	μF	1.00	
3) 265.26	μF		
4) 280.86	μF		
The armat resistance second ma	ure has a per phase synch The line voltage of the fi	nronous reactance of irst machine is adjus V. The machine volta	d to a set of common busbars.  1.  Ω and negligible armature ted to 3300 V and that of the ges are in phase at the instant current per phase will be
1) 16.98 /	A		
2) 29.41 /	4		
3) 33.96 /	4		
4) 58.82 /	Ą		
	5 kW, 4 pole, 50 Hz, Y-cor ue of the machine at full loa		or has full load slip of 4%. The
1) 1.66 N	n		
2) 95.50 1	Nm		
3) 99.47 [	Nm		
4) 624.73	Nm		
	, 2-phase bipolar stepper speed of the motor in rpm is		rate is 100 steps/second. The
1) 15	2) 30	3) 60	4) 90
		10/22	

43. The resistance and reactance of a 100 kVA 11000/ 400 V,  $\Delta$  - Y distribution transformer are 0.02 and 0.07 pu respectively. The phase impedance of the transformer referred to

1) 50.0 kVA 2) 53.5 kVA 3) 717.4 kVA 4) 767.4 kVA

the primary is

1)  $(0.02 + j0.07) \Omega$ 2)  $(0.55 + j1.925) \Omega$ 3)  $(15.125 + j52.94) \Omega$ 4)  $(72.6 + j254.1) \Omega$ 

11/22					
	2) 1650 kV				
	1) 1250 kV				
! \	A lightning stroke disch line having surge imper waves in either direction	dance of 250 $\Omega$ . The m	nagnitude of transient o	over-voltage travelling	
	1) 5.0	2) 31.7	3) 37.8	4) 189.0	
i	dielectric power loss in	nF/km. If the dielect this cable in W/km is	ric loss tangent of XL	PE is 2 x 10 <sup>-4</sup> , then	
3	A 800 kV transmission phase line capacitance transfer capability in MV 1) 1204 MW 2) 1504 MW 3) 2085 MW 4) 2606 MW	e of 11.68 nF/km. Ign Wis	oring the length of the	e line, its ideal power	
	1) 13.43 kA 2) 15.79 kA 3) 23.25 kA 4) 27.36 kA	cn9	IUG		
	A 500 MW 3-phase Y-c 0.85 pf. The line curren			_	
	1) 12.29 A 2) 16.24 A 3) 21.29 A 4) 36.88 A			COL	
;	A 400 V, 50 kVA, 0. synchronous reactance windage losses are 2 ka power factor of 0.8 le	e of <b>2</b> and negligible W and the core loss is	e armature resistance s 0.8 kW. The shaft is s	e. The friction and	
	2) 192 V 3) 384 V 4) 768 V				
	1) 96 V				

48. A 8 pole, DC generator has a simplex wave-wound armature containing 32 coils of 6 turns each. Its flux per pole is 0.06 Wb. The machine is running at 250 rpm. The induced

armature voltage is

- 3) 2500 kV
- 4) 2900 kV
- 54. The generalized circuit constants of a 3-phase, 220 kV rated voltage, medium length transmission line are

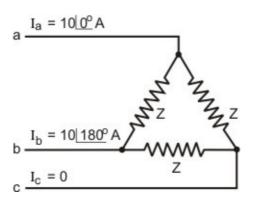
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A = D = 0.936 + j0.016 = 0.936 | 0.98^{\circ}
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B = 
$$33.5 + j138 = 142.0 \ \underline{)76.4}^{\circ} \Omega$$

$$C = (-5.18 + j914) \times 10^{-6} \Omega$$

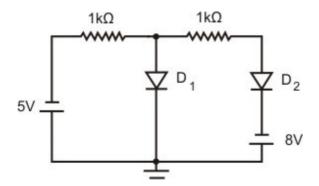
If the load at the receiving end is 50 MW at 220 kV with a power factor of 0.9 lagging, then magnitude of line to line sending end voltage should be

- 1) 133.23 kV
- 2) 220.00 kV
- 3) 230.78 kV
- 4) 246.30 kV
- 55. A new generator having  $E_g=1.4\,\underline{|30\,^\circ}$  pu [equivalent to (1.212 + j0.70) pu] and synchronous reactance 'X<sub>s</sub>' of 1.0 pu on the system base, is to be connected to a bus having voltage V<sub>t</sub> in the existing power system. This existing power system can be represented by Thevenin's voltage  $E_{th}=0.9\,\underline{|0\,^\circ}$  pu in series with Thevenin's impedance  $Z_{th}=0.25\,\underline{|90\,^\circ}$  pu. The magnitude of the bus voltage V<sub>t</sub> of the system in pu will be
  - 1) 0.990
  - 2) 0.973
  - 3) 0.963
  - 4) 0.900
- 56. A 3-phase generator rated at 110 MVA, 11 kV is connected through circuit breakers to a transformer. The generator is having direct axis sub-transient reactance  $X''_d = 19\%$ , transient reactance  $X'_d = 26\%$  and synchronous reactance = 130%. The generator is operating at no load and rated voltage when a three phase short circuit fault occurs between the breakers and the transformer. The magnitude of initial symmetrical rms current in the breakers will be
  - 1) 4.44 kA
  - 2) 22.20 kA
  - 3) 30.39 kA
  - 4) 38.45 kA
- 57. A 3-phase transmission line supplies connected load Z. The conductor 'c' of the line develops an open circuit fault as shown in Figure. The currents in the lines are as shown on the diagram. The +ve sequence current component in line 'a' will be

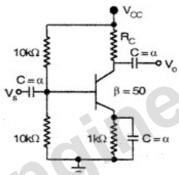


- 1) 5.78 <u>| -30°</u>
- 2) 5.78 <u>| 90°</u>
- 3) 6.33 <u>| 90°</u>
- 4) 10.00 <u>| -30°</u>
- 58. A 500 MVA, 50 Hz, 3-phase turbo-generator produces power at 22 kV. Generator is Y-connected and its neutral is solidly grounded. Its sequence reactances are  $X_1 = X_2 = 0.15$  and  $X_0 = 0.05$  pu. It is operating at rated voltage and disconnected from the rest of the system (no load). The magnitude of the sub-transient line current for single line to ground fault at the generator terminal in pu will be
  - 1) 2.851
  - 2) 3.333
  - 3) 6.667
  - 4) 8.553
- 59. A 50 Hz, 4-pole, 500 MVA, 22 kV turbo-generator is delivering rated megavolt-amperes at 0.8 power factor. Suddenly a fault occurs reducing is electric power output by 40%. Neglect losses and assume constant power input to the shaft. The accelerating torque in the generator in MNm at the time of the fault will be
  - 1) 1.528
  - 2) 1.018
  - 3) 0.848
  - 4) 0.509
- 60. A hydraulic turbine having rated speed of 250 rpm is connected to a synchronous generator. In order to produce power at 50 Hz, the number of poles required in the generator are
  - 1)6

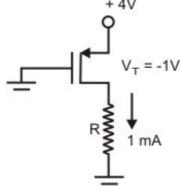
- 2) 12
- 3) 16
- 4) 24
- 61. Assuming that the diodes are ideal in Figure, the current in diode D<sub>1</sub> is



- 1) 8 mA
- 2) 5 mA
- 3) 0 mA
- 4) 3 mA
- 62. The transconductance  $g_m$  of the transistor shown in Figure is 10 mS. The value of the input resistance  $R_{\text{IN}}$  is

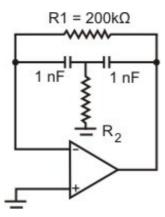


- 1) 10.0 kΩ
- 2) 8.3 kΩ
- 3) 5.0 kΩ
- 4)  $2.5 k\Omega$
- 63. The value of R for which the PMOS transistor in Figure, will be biased in linear region is

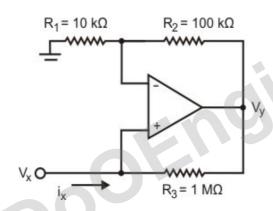


- 1) 220 Ω
- 2) 470 Ω
- 3)  $680 \Omega$
- 4) 1200 Ω

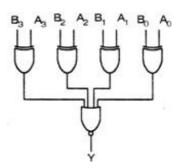
equal to



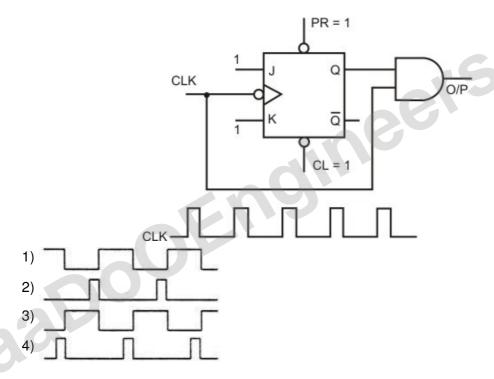
- 1) 1000 rad/s
- 2) 100 rad/s
- 3) 10 rad/s
- 4) 1 rad/s
- eers.com 65. The input resistance  $R_{IN}(=v_X/i_X)$  of the circuit in Figure, is



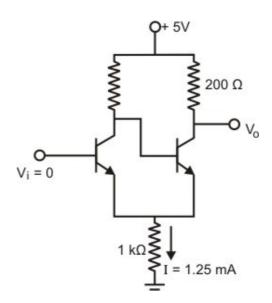
- 1)  $+100 \text{ k}\Omega$
- 2) -100 kΩ
- 3)  $+1 M\Omega$
- 4) -1 MΩ
- 66. The simplified form of the Boolean expression  $Y = (\overline{A} \cdot BC + D)(\overline{A} \cdot D + \overline{B} \cdot \overline{C})$  can be written as
  - 1) A.D+B.C.D
  - 2) AD+B. C.D
  - 3)  $(\overline{A} + D) (\overline{B} \cdot C + \overline{D})$
  - 4)  $A.\overline{D} + BC.\overline{D}$
- 67. A digital circuit which compares two numbers A<sub>3</sub> A<sub>2</sub> A<sub>1</sub> A<sub>0</sub>, B<sub>3</sub> B<sub>2</sub> B<sub>1</sub> B<sub>0</sub> is shown in Figure. To get output Y = 0, choose one pair of correct input numbers



- 1) 1010, 1010
- 2) 0101, 0101
- 3) 0010, 0010
- 4) 0010, 1011
- 68. The digital circuit shown in Figure, generates a modified clock pulse at the output. Choose the correct output waveform from the options given below.



69. In the Schmitt trigger circuit shown in Figure, if  $V_{CE(sat)} = 0.1 \text{ V}$ , the output logic low level  $(V_{OL})$  is



- 1) 1.25 V
- 2) 1.35 V
- 3) 2.50 V
- 4) 5.00 V
- 70. If the following program is executed in a microprocessor, the number of instruction cycles it will take from START to HALT is

START MVI A, 14H; Move 14H to register A

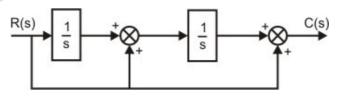
SHIFT RLC; Rotate left without carry

JNZ SHIFT; Jump on non-zero to SHIFT HALT

1) 4

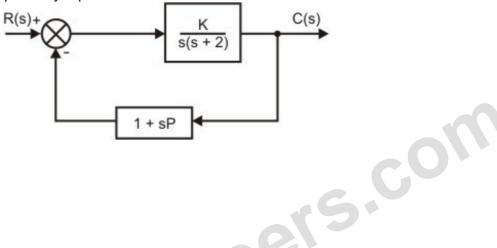
2) 8

- 3) 13
- 4) 16
- 71. For the equation,  $s^3$   $4s^2$  + s + 6 = 0 the number of roots in the left half of s-plane will be
  - 1) zero
- 2) one
- 3) two
- 4) three
- 72. For the block diagram shown in Figure, the transfer function C(s)/R(s) is equal to



- 1)  $(s^2 + 1)/s^2$
- 2)  $(s^2 + s + 1)/s^2$
- 3)  $(s^2 + s + 1)/s$
- 4)  $1/(s^2 + s + 1)$
- 73. The state variable description of a linear autonomous system is, X = AX, where X is the two dimensional state vector and A is the system matrix given by  $A = \begin{bmatrix} 0 & 2 \\ 2 & 0 \end{bmatrix}$ . The roots of the characteristic equation are

- 1) -2 and +2
- 2) j2 and + j2
- 3) -2 and -2
- 4) + 2 and + 2
- 74. The block diagram of a closed loop control system is given by Figure. The values of K and P such that the system has a damping ratio of 0.7 and an undamped natural frequency  $\omega_n$  of 5 rad/sec, are respectively equal to



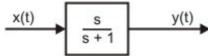
- 1) 20 and 0.3
- 2) 20 and 0.2
- 3) 25 and 0.3
- 4) 25 and 0.2
- 75. The unit impulse response of a second order under-damped system starting from rest is given by

$$c(t) = 12.5 e^{-6t} \sin 8 t, t \ge 0$$

The steady-state value of the unit step response of the system is equal to

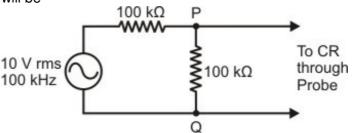
1) 0

- 2) 0.25
- 3) 0.5
- 4) 1.0
- 76. In the system shown in Figure, the input  $x(t) = \sin t$ . In the steady-state, the response y(t) will be

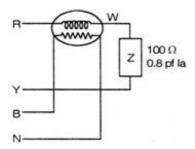


- 1) (1/√2) sin (t 45º)
- 2)  $(1/\sqrt{2}) \sin (t + 45^{\circ})$
- 3) sin (t 45°)
- 4)  $\sin (t + 45^{\circ})$
- 77. The open loop transfer function of a unity feedback control system is given as  $G(s) = (as + 1)/s^2$ . The value of 'a' to give a phase margin of 45° is equal to
  - 1) 0.141
  - 2) 0.441
  - 3) 0.841
  - 4) 1.141
- 78. A CRO probe has an impedance of 500 to in parallel with a capacitance of 10 pF. The

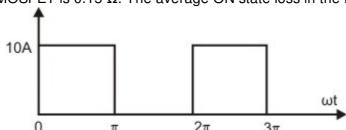
probe is used to measure the voltage between P and Q as shown in Figure. The measured voltage will be



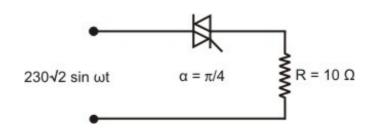
- 1) 3.53 V
- 2) 4.37 V
- 3) 4.54 V
- 4) 5.00 V
- 79. A moving coil of a meter has 100 turns, and a length and depth of 10 mm and 20 mm respectively. It is positioned in a uniform radial flux density of 200 mT. The coil carries a current of 50 mA. The torque on the coil is
  - 1) 200 µNm
  - 2) 100 μNm
  - 3) 2 µNm
  - 4) 1 μNm
- 80. A dc A-h meter is rated for 15 A, 250 V. The meter constant is 14.4 A-sec/rev. The meter constant at rated voltage may be expressed as
  - 1) 3750 rev/kWh
  - 2) 3600 rev/kWh
  - 3) 1000 rev/kWh
  - 4) 960 rev/kWh
- 81. A moving iron ammeter produces a full scale torque of 240  $\mu$ Nm with a deflection of 120° at a current of 10 A. The rate of change of self inductance ( $\mu$ H/ radian) of the instrument at full scale is
  - 1) 2.0 µH/radian
  - 2) 4.8 µH/radian
  - 3) 12.0 µH/radian
  - 4) 114.6 µH/radian
- 82. A single-phase load is connected between R and Y terminals of a 415 V, symmetrical, 3-phase, 4 wire system with phase sequence RYB. A wattmeter is connected in the system as shown in Figure. The power factor of the load is 0.8 lagging. The wattmeter will read



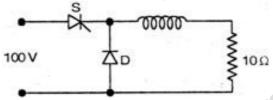
- 1) 795 W
- 2) 597 W
- 3) + 597 W
- 4) + 795 W
- 83. A 50 Hz, bar primary CT has a secondary with 500 turns. The secondary supplies 5 A current into a purely resistive burden of  $\Omega$ . The magnetizing ampere-turns is 200. The phase angle between the primary and secondary current is
  - 1) 4.6°
  - 2) 85.4°
  - 3) 94.6°
  - 4) 175.4°
- 84. A 50 Hz, bar primary CT has a secondary with 500 turns. The secondary supplies 5 A current into a purely resistive burden of  $\Omega$ . The magnetizing ampere-turns is 200. The core flux is
  - 1) 0
  - 2) 45.0 μWb
  - 3) 22.5 mWb
  - 4) 100.0 mWb
- 85. A MOSFET rated for 15 A, carries a periodic current as shown in Figure. The ON state resistance of the MOSFET is 0.15  $\Omega$ . The average ON state loss in the MOSFET is



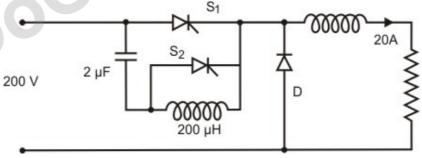
- 1) 33.8 W
- 2) 15.0 W
- 3) 7.5 W
- 4) 3.8 W
- 86. The triac circuit shown in Figure, controls the ac output power to the resistive load. The peak power dissipation in the load is



- 1) 3968 W
- 2) 5290 W
- 3) 7935 W
- 4) 10580 W
- 87. Figure shows a chopper operating from a 100 V dc input. The duty ratio of the main switch S is 0.8. The load is sufficiently inductive so that the load current is ripple free. The average current through the diode D under steady state is

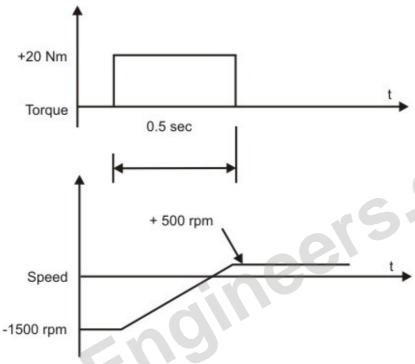


- 1) 1.6 A
- 2) 6.4 A
- 3) 8.0 A
- 4) 10.0 A
- 88. Figure shows a chopper. The device S1 is the main switching device. S2 is the auxiliary commutation device. S1 is rated for 400 V, 60 A. S2 is rated for 400 V, 30 A. The load current is 20 A. The main device operates with a duty ratio of 0.5. The peak current through S1 is



- 1) 10 A
- 2) 20 A
- 3) 30 A
- 4) 40 A
- 89. A single-phase half-controlled rectifier is driving a separately excited dc motor. The dc motor has a back emf constant of 0.5 V /rpm. The armature current is 5 A without any ripple. The armature resistance is **Q**. The converter is working from a 230 V, single phase ac source with a firing angle of 30°. Under this operating condition, the speed of the motor will be

- 1) 339 rpm
- 2) 359 rpm
- 3) 366 rpm
- 4) 386 rpm
- 90. A variable speed drive rated for 1500 rpm, 40 Nm is reversing under no load. Figure, shows the reversing torque and the speed during the transient. The moment of inertia of the drive is



- 1) 0.048 kg m<sup>2</sup>
- 2) 0.064 kg m<sup>2</sup>
- 3) 0.096 kg m<sup>2</sup>
- 4) 0.128 kg m<sup>2</sup>

## **Answer Key**

1) 4	2) 4	3) 3	4) 2	5) 2	6) 3	7) 3	8) 4	9) 3	10) 1	
11) 3	12) 2	13) 3	14) 1	15) 2	16) 3	17) 3	18) 2	19) 1	20) 2	
21) 1	22) 4	23) 3	24) 2	25) 3	26) 3	27) 4	28) 1	29) 2	30) 3	
31) 1	32) 3	33) 1	34) 4	35) 4	36) 1	37) 2	38) 4	39) 1	40) 2	
41) 1	42) 4	43) 4	44) 1	45) 1	46) 3	47) 2	48) 3	49) 3	50) 2	
51) 3	52) 4	53) 1	54) 3	55) 2	56) 3	57) 1	58) 1	59) 1	60) 4	
61) 3	62) 2	63) 4	64) 1	65) 2	66) 1	67) 3	68) 2	69) 2	70) 3	
71) 3	72) 2	73) 1	74) 4	75) 4	76) 2	77) 3	78) 1	79) 1	80) 3	
81) 2	82) 2	83) 1	84) 2	85) 3	86) 4	87) 3	88) 2	89) 3	90) 3	
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3.3	O								70) 3 80) 3 90) 3	