

GATE EC - 2006

Q.1 — Q.20 Carry One Mark Each.

1. The rank of the matrix

$$\begin{bmatrix} 1 & 1 & 1 \\ 1 & -1 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$

is:

$$\begin{bmatrix} 1 & 1 & 1 \\ 1 & -1 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$

- (A) 0
- (B) 1
- (C) 2
- (D) 3

2. $\mathbf{V} \times (\mathbf{V} \times \mathbf{P})$, where \mathbf{P} is a vector, is equal to

- (A) $\mathbf{P} \times \mathbf{V} \times \mathbf{P} - V^2 \mathbf{P}$
- (B) $V^2 \mathbf{P} + \mathbf{V}(\mathbf{V} \cdot \mathbf{P})$
- (C) $V^2 \mathbf{P} + \mathbf{V} \times \mathbf{P}$
- (D) $\mathbf{v}(\mathbf{v} \cdot \mathbf{P}) - v^2 \mathbf{P}$

3. $\int (\mathbf{v} \times \mathbf{P}) \cdot d\mathbf{s}$, where \mathbf{P} is a vector, is equal to

- (A) $4\mathbf{P} \cdot d\mathbf{I}$
- (B) $\mathbf{V} \times \mathbf{V} \times \mathbf{P} \cdot d\mathbf{I}$
- (C) $4\mathbf{V} \times \mathbf{P} \cdot d\mathbf{I}$
- (D) $[[[\mathbf{V} \cdot \mathbf{P} dv$

4. A probability density function is of the form

$$p(x) = Ke^{-ax} \quad x \in \mathbb{R}$$

The value of K is

- (A) 0.5
- (B) 1
- (C) $0.5cL$
- (D) x

5. A solution for the differential equation

$$k(t) + 2x(t) = 5(t)$$

with initial condition $x(0) = 0$ is:

- (A) $e^{-2t}u(t)$
- (B) $e^{2t}u(t)$
- (C) $e^{-t}u(t)$
- (D) $e^{t}u(t)$

6. A low-pass filter having a frequency response $H(j\omega) = \frac{A(\omega)}{1 + j\omega RC}$ does not produce any phase distortion if

- (A) $A(\omega) = C\omega^2, \phi(\omega) = k\omega^3$
- (B) $A(\omega) = C\omega^2, \phi(\omega) = k\omega$
- (C) $A(\omega) = C\omega, \phi(\omega) = k\omega^2$
- (D) $A(\omega) = C, \phi(\omega) = k\omega$

7. The values of voltage (V_3) across a tunnel-diode corresponding to peak and valley currents are V_2 and V_1 respectively. The range of tunnel-diode voltage V_D for which the slope of its IVD characteristics is negative would be

- (A) $V_3 < 0$
- (B) $0 < V_D < V_2$

- (C) $V, V < V$
- (D) $VdVV$

8. The concentration of minority carriers in an extrinsic semiconductor under equilibrium is:

- (A) directly proportional to the doping concentration
- (B) inversely proportional to the doping concentration
- (C) directly proportional to the intrinsic concentration
- (D) inversely proportional to the intrinsic concentration

9. Under low level injection assumption, the injected minority carrier current for an extrinsic semiconductor is essentially the

- (A) diffusion current
- (B) drift current
- (C) recombination current
- (D) induced current

10. The phenomenon known as "Early Effect" in a bipolar transistor refers to a reduction of the effective base-width caused by

- (A) electron-hole recombination at the base
- (B) the reverse biasing of the base-collector junction
- (C) the forward biasing of emitter-base junction
- (D) the early removal of stored base charge during saturation-to-cutoff switching.

11. The input impedance (Z_i) and the output impedance (Z_o) of an ideal transconductance (voltage controlled current source) amplifier are

- (A) $Z_i = 0, Z_o = 0$
- (B) $Z_i = 0, Z_o = \infty$
- (C) $Z_i = \infty, Z_o = 0$
- (D) $Z_i = \infty, Z_o = \infty$

12. An n-channel depletion MOSFET has following two points on its I_D vs V_{GS} curve:

- (i) $V_{GS} = 0$ at $I_D = 12\text{mA}$ and
- (ii) $V_{GS} = -6$ Volts at $I_D = 0$

Which of the following Q-points will give the highest trans-conductance gain for small signals?

- (A) $V_{GS} = -6$ Volts
- (B) $V_{GS} = -3$ Volts
- (C) $V_{GS} = 0$ Volts
- (D) $V_{GS} = 3$ Volts

13. The number of product terms in the minimized sum-of-product expression obtained through the following K-map is (where "d" denotes don't care states)

1001
 0d00
 00d1
 1001

- (A) 2
- (B) 3
- (C) 4

(D) 5

14. The Dirac delta function $\delta(t)$ is defined as

(A) $\delta(t) = 1$ $t=0$.

L° otherwise

100 $t=0$

(B) $\delta(t) =$.

L0 otherwise

(C) $\delta(t) =$. and $\int \delta(t) dt = 1$

L otherwise

(D) $\delta(t) = 4^{\circ\circ}$ $t=0$ and $\int \delta(t) dt = 1$

L otherwise

15. The open-loop transfer function of a unity-gain feedback control system is given by The gain margin of the system in dB is given by

(A) 0

(B) 1

(C) 20

(D)

16. The electric field of an electromagnetic wave propagating in the positive z direction is given by

$$E = a \sin(at - flz) + a \sin ot - flz + .$$

The wave is

(A) linearly polarized in the z-direction

(B) elliptically polarized

(C) left-hand circularly polarized

(D) right-hand circularly polarized

17. A transmission line is feeding 1 Watt of power to a horn antenna having a gain of 10 dB. The antenna is matched to the transmission line. The total power radiated by the horn antenna into the free-space is:

(A) 10 Watts

(B) 1 Watt

(C) 0.1 Watt

(D) 0.01 Watt

18. The eigenvalues and the corresponding eigenvectors of a 2 x 2 matrix are given by Eigenvalue Eigenvector

A1=8

A2=4 v2=[h/l]

The matrix is:

(A) 6 2 L2 6

(B) 6 L6 4

(C) r L 2

(D) 8 L8 4

19. For the function of a complex variable $W = \ln Z$

(where, $W = u + jv$ and $Z = x + jy$), the $u = \text{constant}$ lines get mapped in Z-plane as

(A) set of radial straight lines

(B) set of concentric circles

- (C) set of confocal hyperbolas
 (D) set of confocal ellipses

20. Three companies, X, Y and Z supply computers to a university. The percentage of computers supplied by them and the probability of those being defective are tabulated below. Given that a computer is defective, the probability that it was supplied by Y is:

- (A) 0.1
 (B) 0.2
 (C) 0.3
 (D) 0.4

21. For the matrix [j] the eigenvalue corresponding to the eigenvector is:

- (A) 2
 (B) 4
 (C) 6
 (D) 8

22. For the differential equation $y'' + k^2y = 0$ the boundary conditions are

Company	% of computers supplied	Probability of being defective
X	60%	0.01
Y	30%	0.02
Z	10%	0.03

(i) $y=0$ for $x=0$ and

(ii) $y=0$ for $x=a$

The form of non-zero solutions of y (where m varies over all integers) are m, rx

(A) $y = A \sin mx$

$m a$

m, rx

(B) $y = A \cos mx$

$m a$

(C) $y = 4m$

mrx

(D) $y = A \sin mx$

23. Consider the function $f(t)$ having Laplace transform

$$\frac{2}{s^2 + a^2}, \text{Re}[s] > 0$$

$s + a > 0$

The final value of $f(t)$ would be:

(A) 0

(B) 1

(C) $\frac{1}{a}$

(D)

24. As x is increased from $-\infty$ to ∞ , the function

e^x

$f(x) =$

$1 + e^x$

- (A) monotonically increases
- (B) monotonically decreases
- (C) increases to a maximum value and then decreases
- (D) decreases to a minimum value and then increases

25. The first and the last critical frequencies (singularities) of a driving point impedance function of a passive network having two kinds of elements, are a pole and a zero respectively. The above property will be satisfied by

- (A) RL network only
- (B) RC network only
- (C) LC network only
- (D) RC as well as RL networks

26. In the figure shown below, assume that all the capacitors are initially uncharged. If

$v_o(t) = I_0 u(t)$ Volts, $v_0(t)$ is given by

- (A) $8e^{-t/RC}$ Volts
- (B) $8(1 - e^{-t/RC})$ Volts
- (C) $8u(t)$ Volts
- (D) 8 Volts

27. Consider two transfer functions

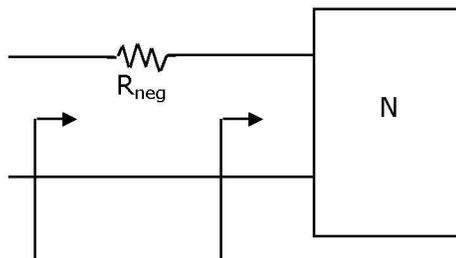
$G_1(S) = \frac{s^2 + as + b}{s^2 + cs + d}$ and $G_2(S) = \frac{s^2 + as + b}{s^2 + es + f}$

$V_o(t)$

The 3-dB bandwidths of their frequency responses are, respectively

- (A) $\frac{1}{\sqrt{a^2 + 4b}}, \frac{1}{\sqrt{a^2 + 4d}}$
- (B) $\frac{1}{\sqrt{a^2 + 4b}}, \frac{1}{\sqrt{a^2 + 4f}}$

28. A negative resistance R_{neg} is connected to a passive network N having driving point impedance $Z_1(s)$ as shown below. For $Z_2(s)$ to be positive real, $Z_2(s)$

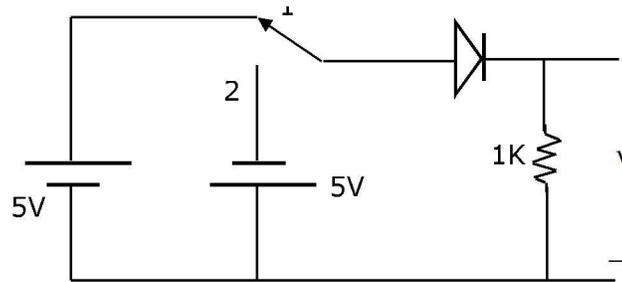


- (A) $R < \text{Re} Z_1(j\omega), V_a \text{ neg}$
- (B) $R < \text{Im} Z_1(j\omega), V_a \text{ neg}$
- (C) $R < \text{Im} Z_1(j\omega), V_a \text{ neg}$
- (D) $R < \text{Re} Z_1(j\omega), V_a \text{ neg}$

29. In the circuit shown below, the switch was connected to position 1 at $t < 0$ and at $t = 0$, it is changed to position 2. Assume that the diode has zero voltage drop and a storage time t_s .

For $0 < t < t_s$, v is given by (all in Volts)

- (A) $v = -5$
- (B) $v = -5$



(D) $-5 < v < 0$

30. The majority carriers in an n-type semiconductor have an average drift velocity v in a direction perpendicular to a uniform magnetic field B . the electric field E induced due to Hall effect acts in the direction

- (A) $v \times B$
- (B) $B \times v$
- (C) along v
- (D) opposite to v

31. A heavily doped n-type semiconductor has the following data:

Hole-electron mobility ratio : 0.4

Doping concentration : 4.2×10^8 atoms/m³

Intrinsic concentration : 1.5×10 atoms/m³

The ratio of conductance of the n-type semiconductor to that of the intrinsic semiconductor of same material and at the same temperature is given by

- (A) 0.00005
- (B) 2,000
- (C) 10,000
- (D) 20,000

32. For the circuit shown below; assume that the zener diode is ideal with a breakdown voltage of 6 Volts. The waveform observed across R is:

- (A) 6V
- (B) $I_2 \sin \omega t$ R VR
- (C) 12V



33. A new Binary Coded Pentary (BCP) number system is proposed in which every digit of a base-5 number is represented by its corresponding 3-bit binary code.

For example, the base-5 number 24 will be represented by its BCP code 010100.
 In this numbering system, the BCP code 100010011001 corresponds to the following number in base-5 system

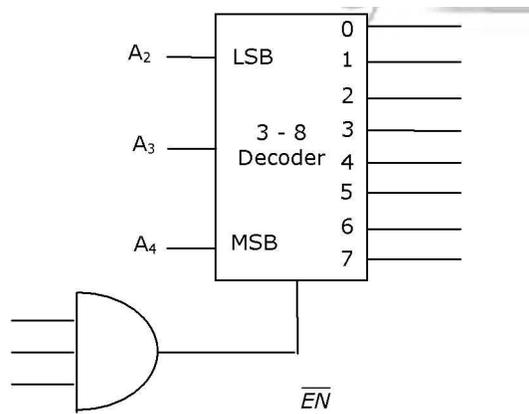
- (A) 423
- (B) 1324
- (C) 2201
- (D) 4231

34. An I/O peripheral device shown in figure (b) below is to be interfaced to an 8085 microprocessor. To select the I/O device in the I/O address range D4 H — D7 H, its chip-select (Cs) should be connected to the output of the decoder shown in figure (a) below:

I/O

Peripheral

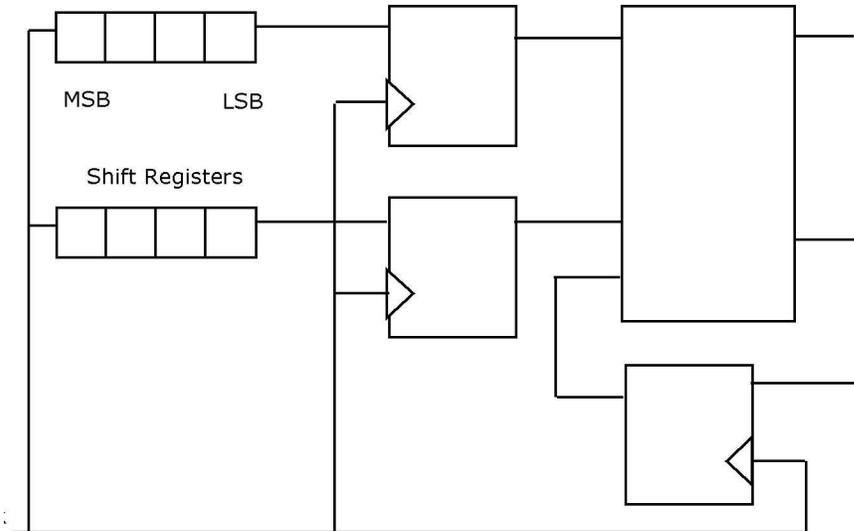
- (B) output 5
- (C) output 2
- (D) output 0



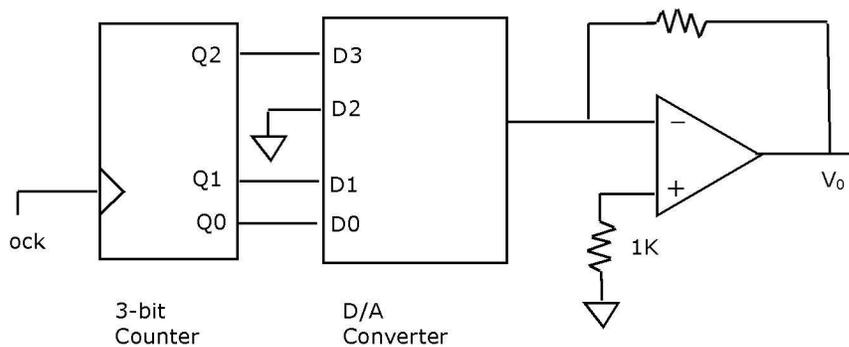
35. A 4-bit D/A converter is connected to a free-running 3-bit UP counter, as shown in the following figure. Which of the following waveforms will be observed at V_3 ? the flip-flops are in clear state. After applying two clock pulses, the outputs of the full-adder should be

Clock

- (A) S=0 C0
- (B) S=0 C0
- (C) S=1 C0
- (D) S=1 C0



36. Two D-flip-flops, as shown below, are to be connected as a synchronous counter that goes through the following Q_1Q_0 sequence
 00 – 01 – 11 – 10 – 00 –
 The inputs D_0 and D_1 respectively should be connected as



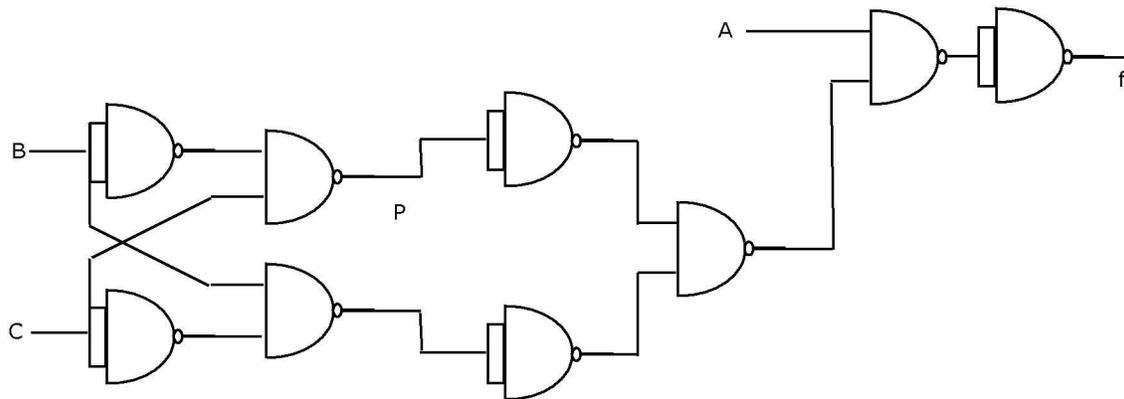
- (A) Q_1 and Q_0
- (B) Q_0 and Q_1
- (C) Q_1Q_0 and Q_1Q_0
- (D) and Q_1Q_0

37. Following is the segment of a 8085 assembly language program:
 LXI SP, EFFF H
 CALL 3000 H
 3000 H : LXI H, 3CF4 H
 PUSH PSW
 SPHL
 POP PSW
 RET

On completion of RET execution, the contents of SP is:

- (A) 3CFO H
- (B) 3CF8 H
- (C) 3FFD H
- (D) EFFF H

38. The point P in the following figure is stuck-at-i. The output f will be



- (A) ABC
- (B) A
- (C) ABC
- (D) A

39. A signal $m(t)$ with bandwidth 500 Hz is first multiplied by a signal $g(t)$ where $g(t) = \cos(2\pi \cdot 0.5 \times 10^4 t)$

The resulting signal is then passed through an ideal lowpass filter with bandwidth i kHz. The output of the lowpass filter would be:

- (A) $5(t)$
- (B) $m(t)$
- (C) 0
- (D) $m(t)(t)$

40. The minimum sampling frequency (in samples/sec) required to reconstruct the following signal from its samples without distortion.

$$x(t) = 5 \cos(2\pi \cdot 1000t) \sin(2\pi \cdot 1000t^2)$$

$x(t) = 5 \cos(2\pi \cdot 1000t) \sin(2\pi \cdot 1000t^2)$

$Tt \}$

- (A) 2×10^3
- (B) 4×10^3
- (C) 6×10^3
- (D) 8×10^3

41. A uniformly distributed random variable X with probability density function

$$f(x) = \frac{1}{10} (u(x+5) - u(x-5))$$

Where $u(\cdot)$ is the unit step function is passed through a transformation given in the figure

below. The probability density function of the transformed random variable Y would be

- (A) $f(y) = (u(y+2.5) - u(y-2.5))$
- (B) $f(y) = 0.5Y(y) + 0.5Y(y-1)$
- (C) $f(y) = 0.255(y+2.5) + 0.255(y-2.5) + 0.55(y)$
- (D) $f(y) = 0.258(y+2.5) + 0.258(y-2.5) + (u(y+2.5) - u(y-2.5))$

42. A system with input $x[n]$ and output $y[n]$ is given as $y[n] = \sin n x[n]$. The system is:

- (A) linear, stable and invertible
- (B) non-linear, stable and non-invertible
- (C) linear, stable and non-invertible
- (D) linear, unstable and invertible

43. The unit-step response of a system starting from rest is given by $c(t) = 1 - e^{-2t}$ for $t \geq 0$

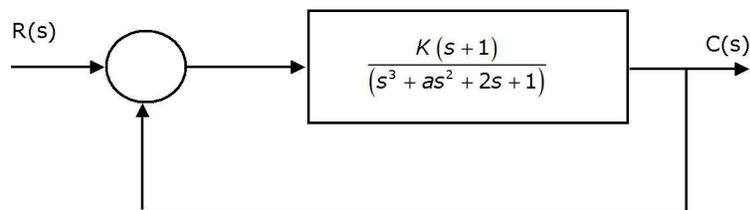
The transfer function of the system is:

- (A) $1 + 2s$
- (B) $2 + s$
- (C) $2 + s$
- (D) $2s + 1 + 2s$

44. The Nyquist plot of $G(j\omega)H(j\omega)$ for a closed loop control system, passes through $(-1, j0)$ point in the GH plane. The gain margin of the system in dB is equal to

- (A) infinite
- (B) greater than zero
- (C) less than zero
- (D) zero

45. The positive values of "K" and "a" so that the system oscillates at a frequency of 2 rad/sec respectively are shown in the figure below



- (A) 1, 0.75
- (B) 2, 0.75
- (C) 1, 1
- (D) 2, 2

46. The unit impulse response of a system is:

For this system, the steady-state value of the output for unit step input is equal to

- (A) -1

- (B) 0
- (C) 1
- (D)

47. A linear system is described by the following state equation

$$\dot{x}(t) = Ax(t) + Bu(t), \quad A = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

The state-transition matrix of the system is:

- (A) $\begin{bmatrix} \cos t & \sin t \\ -\sin t & \cos t \end{bmatrix}$
- (B) $\begin{bmatrix} \cos t & \sin t \\ \sin t & -\cos t \end{bmatrix}$
- (C) $\begin{bmatrix} \cos t & -\sin t \\ \sin t & \cos t \end{bmatrix}$
- (D) $\begin{bmatrix} \cos t & -\sin t \\ \cos t & \sin t \end{bmatrix}$

48. The minimum step-size required for a Delta-Modulator operating at 32 K samples/sec to track the signal (here $u(t)$ is the unit-step function)

$$x(t) = 125t(u(t) - u(t-1)) + (250 - 125t)(u(t-1) - u(t-2))$$

So that slope-overload is avoided, would be

- (A) 2 10
- (B) 2 8
- (C) 2 6
- (D) 2

49. A zero-mean white Gaussian noise is passed through an ideal lowpass filter of bandwidth 10 kHz. The output is then uniformly sampled with sampling period $t = 0.03$ msec. The samples so obtained would be

- (A) correlated
- (B) statistically independent
- (C) uncorrelated
- (D) orthogonal

50. A source generates three symbols with probabilities 0.25, 0.25, 0.50 at a rate of 3000 symbols per second. Assuming independent generation of symbols, the most efficient source encoder would have average bit rate as

- (A) 6000 bits/sec
- (B) 4500 bits/sec
- (C) 3000 bits/sec
- (D) 1500 bits/sec

51. The diagonal clipping in Amplitude Demodulation (using envelope detector) can be avoided if RC time-constant of the envelope detector satisfies the following condition, (here W is message bandwidth and ω_c is carrier frequency both in rad/sec)

- (A) $RC \ll \frac{1}{W}$
- (B) $RC \gg \frac{1}{W}$
- (C) $RC \ll \frac{1}{\omega_c}$
- (D) $RC \gg \frac{1}{\omega_c}$

52. A message signal with bandwidth 10 kHz is Lower-Side Band SSB modulated with carrier frequency $f_c = 10$ Hz: The resulting signal is then passed through a

Narrow-Band Frequency Modulator with carrier frequency $f_c = 10^8$ Hz.

The bandwidth of the output would be:

- (A) 4×10^4 Hz
- (B) 2×10^6 Hz
- (C) 2×10^9 Hz
- (D) 2×10^{10} Hz

53. A medium of relative permittivity $\epsilon_r = 2$ forms an interface with free-space. A point source of electromagnetic energy is located in the medium at a depth of 1 meter from the interface. Due to the total internal reflection, the transmitted beam has a circular cross-section over the interface. The area of the beam cross-section at the interface is given by

- (A) $2\pi \text{ m}^2$
- (B) $\pi \text{ m}^2$
- (C) $\pi \text{ m}^2$
- (D) $2\pi \text{ m}^2$

54. A medium is divided into regions I and II about $x = 0$ plane, as shown in the figure below. An electromagnetic wave with electric field $E_1 = 4a_x + 3a_y + 5a_z$ is incident normally on the interface from region-I. The electric field E_2 in region-II at the interface is:

Region I Region II

$\epsilon_1 = 4$ $\epsilon_2 = 1$

$E_1 =$

$x < 0$ $x = 0$ $x > 0$

- (A) $E_2 = E_1$
- (B) $4a_x + 0.75a_y - 1.25a_z$
- (C) $3a_x + 3a_y + 5a_z$
- (D) $-3a_x + 3a_y + 5a_z$

54. A rectangular waveguide having TE_{10} mode as dominant mode is having a cutoff frequency of 18-GHz for the TE_{30} mode. The inner broad-wall dimension of the rectangular waveguide is:

- (A) 5 cm
- (B) 5 cm
- (C) 8 cm
- (D) 10 cm

55. A mast antenna consisting of a 50 meter long vertical conductor operates over a perfectly conducting ground plane. It is base-fed at a frequency of 600 kHz. The radiation resistance of the antenna in Ohms is:

- (A) 20π
- (B) 20π
- (C) 20π
- (D) 20π

Common Data Questions:

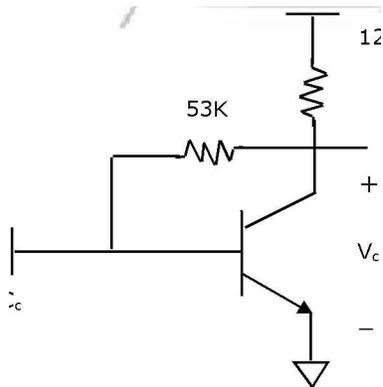
Common Data for Questions 71, 72, 73:

In the transistor amplifier circuit shown in the following parameters:

$I_{DC} = 60 \mu\text{A}$, $\beta_{FE} = 0.7$, $h_{ie} = 100$, $h_{fe} = 70$. The capacitance C_{in} can be assumed to be infinite.

5.3K

figure below, the transistor has the $\beta = 100$

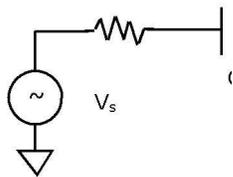


In the figure above, the ground has been shown by the symbol ∇

71. Under the DC conditions, the collector-to-emitter voltage drop is:

- (A) 4.8 Volts
- (B) 5.3 Volts
- (C) 6.0 Volts
- (D) 6.6 Volts

72. If I_{BDC} is increased by 10%, the collector-to-emitter voltage drop



- (A) increases by less than or equal to 10%
- (B) decreases by less than or equal to 10%
- (C) increases by more than 10%
- (D) decreases by more than 10%

73. The small-signal gain of the amplifier v_o/v_i is:

- (A) -10
- (B) -5.3
- (C) 5.3
- (D) 10

Common Data for Questions 74, 75:

Let $g(t) = p(t) * p(t)$, where $*$ denotes convolution and $p(t) = u(t) - u(t-1)$ with $u(t)$ being the unit step function

74. The impulse response of filter matched to the signal $s(t) = g(t) - 2 * g(t)$ is given as:

- (A) $s(1-t)$
- (B) $-s(1-t)$ T EForum
- (C) $-s(t)$
- (D) $s(t)$

75. An Amplitude Modulated signal is given as

$$XAM(t) = 100(p(t) + 0.5g(t))\cos at$$

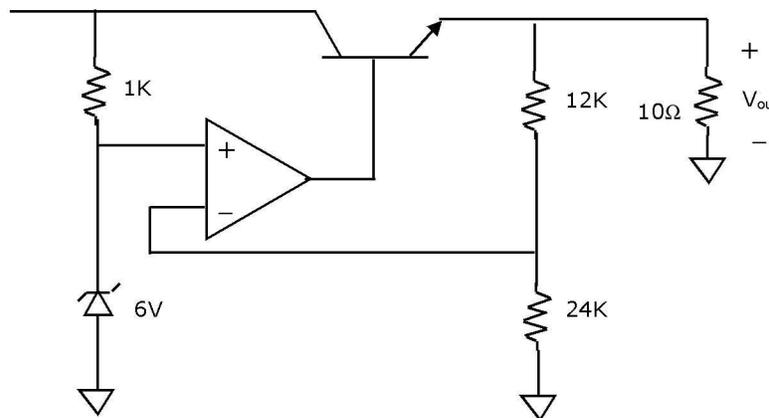
in the interval $0 < t < 1$. One set of possible values of the modulating signal and modulation index would be

- (A) $t, 0.5$
- (B) $t, 1.0$
- (C) $t, 2.0$
- (D) $t, 0.5$

Linked Answer Questions: Q.76 to Q.85 Carry Two Marks Each.

Statement for Linked Answer Questions 76 & 77:

A regulated power supply, shown in figure below, has an unregulated input (UR) of 15 Volts and generates a regulated output Use the component values shown in the figure.



In the figure above, the ground has been shown by the symbol ∇

76. The power dissipation across the transistor Q_1 shown in the figure is:

- (A) 4.8 Watts
- (B) 5.0 Watts
- (C) 5.4 Watts
- (D) 6.0 Watts

77. If the unregulated voltage increases by 20%, the power dissipation across the transistor Q_1

- (A) increases by 20%
- (B) increases by 50%
- (C) remains unchanged
- (D) decreases by 20%

Statement for Linked Answer Questions 78 & 79:

The following two questions refer to wide sense stationary stochastic processes

78. It is desired to generate a stochastic process (as voltage process) with power spectral density $S_x(f)$ by driving a Linear-Time-Invariant system by zero mean white noise (as voltage process) with power spectral density being constant equal to 1. The system which can perform the desired task could be:

- (A) first order lowpass R-L filter
- (B)
- (C)
- (D)

Statement for Linked Answer Questions 80 & 81:

Consider the following Amplitude Modulated (AM) signal, where $m < B$:

$$x_{AM}(t) = 10(1 + 0.5\sin 2\pi f_m t)\cos 2\pi f_c t$$

average side band power of the AM signal given above is:

81. The AM signal gets added to a noise with Power Spectral Density $S_n(f)$ given in the figure below. The ratio of average sideband power to mean noise power would be:

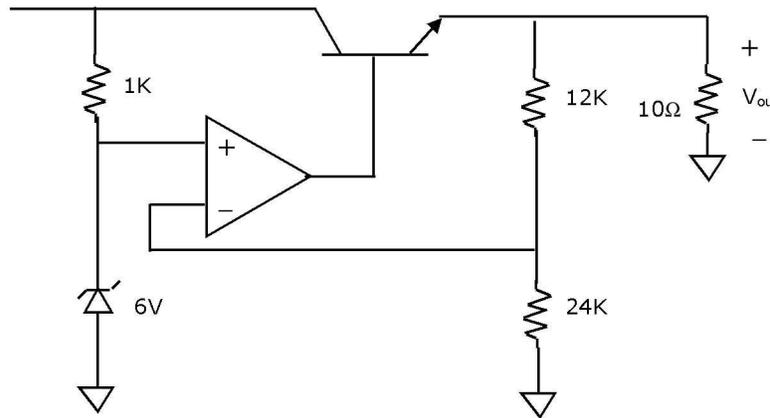
- (A) 25
- (B) 12.5
- (C) 6.25
- (D) 3.125

Statement for Linked Answer Questions 82 & 83:

Consider a unity-gain feedback control system whose open-loop transfer function is:

first order highpass R-C filter

series R-L-C filter



82. The value of "a" so that the system has a phase margin equal to -is approximately equal to

- (A) 2.40
- (B) 1.40
- (C) 0.84
- (D) 0.74

83. With the value of "a" set for a phase-margin of the value of unit-impulse response of the open-loop system at $t = 1$ second is equal to

- (A) 3.40
- (B) 2.40
- (C) 1.84
- (D) 1.74

Statement for Linked Answer Questions 84 & 85:

A 30-Volts battery with zero source resistance is connected to a coaxial line of characteristic impedance of 50 Ohms at $t = 0$ second terminated in an unknown resistive load. The line length is that it takes 400 ps for an electromagnetic wave to travel from source end to load end and vice-versa. At $t = 400$ ps, the voltage at the load end is found to be 40 Volts.

84. The load resistance is

- (A) 25 Ohms
- (B) 50 Ohms
- (C) 75 Ohms
- (D) 100 Ohms

85. The steady-state current through the load resistance is:

- (A) 1.2 Amps
- (B) 0.3 Amps
- (C) 0.6 Amps
- (D) 0.4 Amps

