

ELECTRONICS & COMMUNICATION ENGINEERING

ONE MARKS QUESTIONS

1. The values of voltage (V_D) across a tunnel-diode corresponding to peak and valley currents are V_p and V_v respectively. The range of tunnel-diode voltage V_D for which the slope of its $I-V_D$ characteristics is negative would be
 - a. $V_D < 0$
 - b. $0 \leq V_D < V_p$
 - c. $V_p \leq V_D < V_v$
 - d. $V_D \geq V_v$
2. The concentration of minority carriers in an extrinsic semiconductor under equilibrium is
 - a. directly proportional to the doping concentration
 - b. inversely proportional to the doping concentration
 - c. directly proportional to the intrinsic concentration
 - d. inversely proportional to the intrinsic concentration
3. Under low level injection assumption, the injected minority carrier current for an extrinsic semiconductor is essentially the
 - a. diffusion current
 - b. drift current
 - c. recombination current
 - d. induced current
4. The phenomenon known as "Early Effect" in a bipolar transistor refers to a reduction of the effective base-width caused by
 - a. electron-hole recombination at the base
 - b. the reverse biasing of the base-collector junction
 - c. the forward biasing of emitter-base junction
 - d. the early removal of stored base charge during saturation-to-cutoff switching
5. The input impedance (Z_i) and the output impedance (Z_o) of an ideal transconductance (voltage controlled current source) amplifier are
 - a. $Z_i = 0, Z_o = 0$
 - b. $Z_i = 0, Z_o = \infty$
 - c. $Z_i = \infty, Z_o = 0$
 - d. $Z_i = \infty, Z_o = \infty$
6. An n-channel depletion MOSFET has following two points on its I_D-V_{GS} curve:
 1. $V_{GS} = 0$ at $I_D = 12\text{mA}$ and
 2. $V_{GS} = -6\text{ Volts}$ at $Z_o = \infty$
 Which of the following Q-points will give the highest trans-conductance gain for small signals?
 - a. $V_{GS} = -6\text{ Volts}$
 - b. $V_{GS} = -3\text{ Volts}$
 - c. $V_{GS} = 0\text{ Volts}$
 - d. $V_{GS} = 3\text{ Volts}$
7. The number of product terms in the minimized sum-of-product expression obtained through the following K-map is (where, "d" denotes don't care states)

1	0	0	1
0	d	0	0
0	0	d	1
1	0	0	1

 - a. 2
 - b. 3
 - c. 4
 - d. 5
8. Let $x(t) \leftrightarrow X(j\omega)$ be Fourier Transform pair. The Fourier Transform of the signal $x(5t - 3)$ in terms of $X(j\omega)$ is given as
 - a. $\frac{1}{5} e^{-\frac{j3\omega}{5}} X\left(\frac{j\omega}{5}\right)$
 - b. $\frac{1}{5} e^{\frac{j3\omega}{5}} X\left(\frac{j\omega}{5}\right)$
 - c. $\frac{1}{5} e^{-j3\omega} X\left(\frac{j\omega}{5}\right)$
 - d. $\frac{1}{5} e^{j3\omega} X\left(\frac{j\omega}{5}\right)$
9. The Dirac delta function $\delta(t)$ is defined as
 - a. $\delta(t) = \begin{cases} 1 & t = 0 \\ 0 & \text{otherwise} \end{cases}$

$$b. \delta(t) = \begin{cases} \infty & t=0 \\ 0 & \text{otherwise} \end{cases}$$

$$c. \delta(t) = \begin{cases} 1 & t=0 \\ 0 & \text{otherwise} \end{cases} \text{ and } \int_{-\infty}^{\infty} \delta(t) dt = 1$$

$$d. \delta(t) = \begin{cases} \infty & t=0 \\ 0 & \text{otherwise} \end{cases} \text{ and } \int_{-\infty}^{\infty} \delta(t) dt = 1$$

10. If the region of convergence of $x_1[n] + x_2[n]$ is $\frac{1}{3} < |z| < \frac{2}{3}$, then the region of convergence of $x_1[n] - x_2[n]$ includes

$$a. \frac{1}{3} < |z| < 3$$

$$b. \frac{2}{3} < |z| < 3$$

$$c. \frac{3}{2} < |z| < 3$$

$$d. \frac{1}{3} < |z| < \frac{2}{3}$$

11. The open-loop transfer function of a unity-gain feedback control system is given by

$$G(s) = \frac{K}{(s+1)(s+2)}$$

The gain margin of the system in dB is given by

$$a. 0$$

$$b. 1$$

$$c. 20$$

$$d. \infty$$

12. In the system shown below $x(t) = (\sin t)u(t)$. It steady-state, the response $y(t)$ will be



$$a. \frac{1}{\sqrt{2}} \sin\left(t - \frac{\pi}{4}\right)$$

$$b. \frac{1}{\sqrt{2}} \sin\left(t + \frac{\pi}{4}\right)$$

$$c. \frac{1}{\sqrt{2}} e^t \sin t$$

$$d. \sin t - \cos t$$

13. The electric field of an electromagnetic wave propagating in the positive z-direction is given by

$$E = a_x \sin(\omega t - \beta z) + a_y \sin(\omega t - \beta z + \pi/2)$$

The wave is

a. linearly polarized in the z-direction

b. elliptically polarized

c. left-hand circularly polarized

d. right-hand circularly polarized

14. A transmission line is feeding 1 Watt of power to a horn antenna having a gain of 10dB. The antenna is matched to the transmission line. The total power radiated

a. 10 Watts

b. 1 Watt

c. 0.1 Watt

d. 0.01 Watt

15. The rank of the matrix $\begin{bmatrix} 1 & 1 & 1 \\ 1 & -1 & 0 \\ 1 & 1 & 1 \end{bmatrix}$ is

a. 0

b. 1

c. 2

d. 3

16. $\nabla \times \nabla \times P$, where P is a vector is equal to

$$a. P \times \nabla \times P - \nabla^2 P$$

$$b. \nabla^2 P \times \nabla P (\nabla P)$$

$$c. \nabla^2 P + \nabla \times P$$

$$d. \nabla(\nabla P) - \nabla^2 P$$

17. $\iint (\nabla \times P) \cdot ds$, Where P is a vector, is equal to

$$a. \oint P \cdot dl$$

$$b. \oint \nabla \times \nabla \times p \cdot dl$$

$$c. \oint \nabla \times p \cdot dl$$

$$d. \iiint \nabla p \cdot dv$$

18. A probability density function is of the form

$$p(x) = K e^{-\alpha|x|}, x \in (-\infty, \infty)$$

The value of K is

$$a. 0.5$$

$$b. 1$$

$$c. 0.5\alpha$$

$$d. \alpha$$

19. A solution for the differential equation

$$\dot{x}(t) + 2x(t) = \delta(t)$$

with initial condition $x(0^-) = 0$ is

- a. $e^{-2t} u(t)$
- b. $e^{2t} u(t)$
- c. $e^{-t} u(t)$
- d. $e^t u(t)$

20. A low-pass filter having a frequency response $H(j\omega) = A(\omega)e^{j\phi(\omega)}$ does not produce any phase distortion if

- a. $A(\omega) = C\omega^{-1}, \phi(\omega) = k\omega^2$
- b. $A(\omega) = C\omega^{-2}, \phi(\omega) = k\omega$
- c. $A(\omega) = C\omega, \phi(\omega) = k\omega^2$
- d. $A(\omega) = C, \phi(\omega) = k\omega^{-1}$

TWO MARKS QUESTIONS

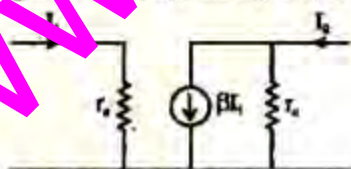
21. A two-port network is represented by ABCD parameters given by

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

If port-2 is terminated by R_L , the input impedance seen at port-1 is given by

- a. $\frac{A + BR_L}{C + DR_L}$
- b. $\frac{AR_L + C}{BR_L + D}$
- c. $\frac{DR_L + A}{BR_L + C}$
- d. $\frac{B + AR_L}{D + CR_L}$

22. In the two port network shown in the figure below, z_{12} and z_{21} are, respectively



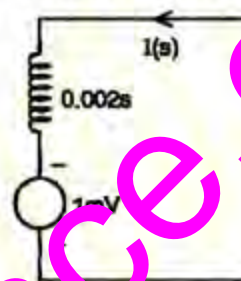
- a. r_0 and βr_0
- b. 0 and $-\beta r_0$
- c. 0 and βr_0
- d. r_0 and $-\beta r_0$

23. The first and the last critical frequencies (singularities) of a driving point

impedance function of a passive network having two kinds of elements, are a pole and a zero respectively. The above property will be satisfied by

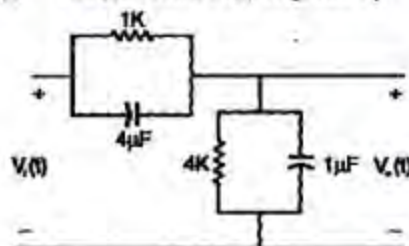
- a. RL network only
- b. RC network only
- c. LC network only
- d. RC as well as RL networks

24. A 2 mH inductor with some initial current can be represented as shown below, where s is the Laplace Transform variable. The value of initial current is



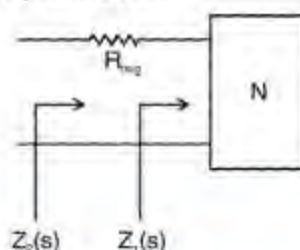
- a. 5 A
- b. 7.0 A
- c. 1.0 A
- d. 0.0 A

25. In the figure shown below, assume that all the capacitors are initially uncharged. If $v_1(t) = 10u(t)$ Volts, $v_0(t)$ is given by



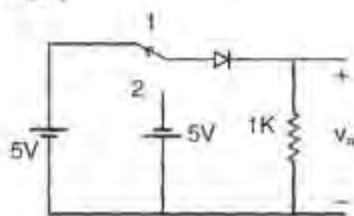
- a. $8e^{-10,000t}$ Volts
- b. $8(1 - e^{-10,000t})$ Volts
- c. $8u(t)$ Volts
- d. 8 Volts

26. A negative resistance R_{neg} is connected to a passive network N having driving point impedance as shown below. For $Z_2(s)$ to be positive real,



- a. $|R_{neg}| \leq \operatorname{Re} Z_1(j\omega), \forall \omega$
 b. $|R_{neg}| \leq |Z_1(j\omega)|, \forall \omega$
 c. $|R_{neg}| \leq \operatorname{Im} Z_1(j\omega), \forall \omega$
 d. $|R_{neg}| \leq \angle Z_1(j\omega), \forall \omega$

27. In the circuit shown below, the switch was connected to position 1 at $t < 0$ and at $t = 0$, it is changed to position 2. Assume that the diode has zero voltage drop and a storage time t_s . For $0 < t \leq t_s$, V_R is given by (all in Volts)



- a. $V_R = -5$
 b. $V_R = +5$
 c. $0 \leq V_R < 5$
 d. $-5 < V_R < 0$
28. The majority carriers in an n-type semiconductor have an average drift velocity v in a direction perpendicular to a uniform magnetic field B . The electric field E induced due to Hall effect acts in the direction
- a. $v \times B$
 b. $B \times v$
 c. along v
 d. opposite to v
29. Find the correct match between Group 1 and Group 2

Group 1

- A. Varactor diode
 B. PIN diode
 C. Zener diode
 D. Schottky diode

Group 2

1. Voltage reference
 2. High-frequency switch
 3. Tuned circuits
 4. Current controlled attenuator

Codes:

	A	B	C	D
a.	4	2	1	3
b.	2	4	1	3
c.	3	4	1	2
d.	1	3	2	4

30. A heavily doped n-type semiconductor has the following data:

Hole-electron mobility ratio : 0.4

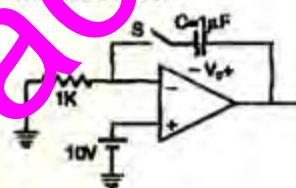
Doping concentration: 4.2×10^{18} atoms / m^3

Intrinsic concentration: 1.5×10^8 atoms / m^3

The ratio of conductance of the n-type semiconductor to that of the intrinsic semiconductor of same material and at the same temperature is given by

- a. 0.00005
 b. 2,000
 c. 10,000
 d. 20,000

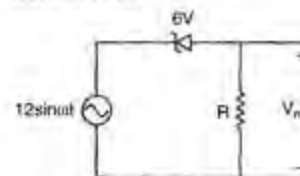
31. For the circuit shown in the following figure, the capacitor C is initially uncharged. At $t = 0$ the switch S is closed. The voltage across the capacitor at $t = 1$ millisecond is



In the figure shown above, the OP AMP is supplied with $\pm 15V$.

- a. 0 Volt
 b. 6.3 Volts
 c. 9.45 Volts
 d. 10 Volts

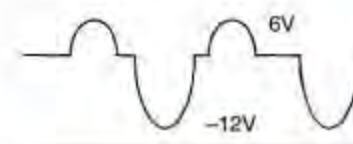
32. For the circuit shown below, assume that the zener diode is ideal with a breakdown voltage of 6 volts. The waveform observed across R is

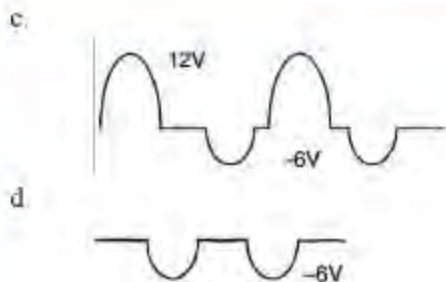


a.



b.



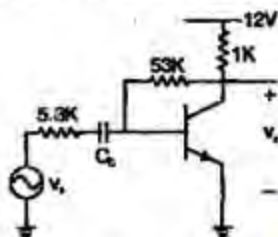


Common Data for Questions 33, 34, 35:

In the transistor amplifier circuit shown in the figure below, the transistor has the following parameters:

$$\beta_{DC} = 60, V_{BE} = 0.7V, h_{ie} \rightarrow \infty, g_{re} \rightarrow \infty$$

The capacitors C_C can be assumed to be infinite.



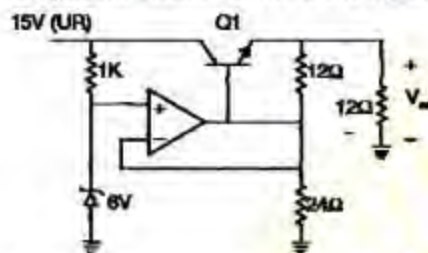
In the figure above, the ground has been shown by the symbol ∇ .

33. Under the DC conditions, the collector-emitter voltage drop is:
- 4.8 Volts
 - 5.3 Volts
 - 6.0 Volts
 - 6.6 Volts
34. If β_{DC} is increased by 10%, the collector-to-emitter voltage drop:
- increases by less than or equal to 10%
 - decreases by less than or equal to 10%
 - increases by more than 10%
 - decreases by more than 10%
35. The small-signal gain of the amplifier v_o/v_i is:
- 10
 - 5.3
 - 5.3
 - 10

Common Data for Questions 36 & 37:

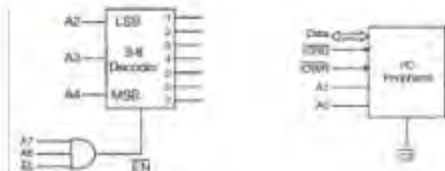
A regulated power supply, shown in figure below, has an unregulated input (UR) of 15 Volts and

generates a regulated output V_{out} . Use the component values shown in the figure



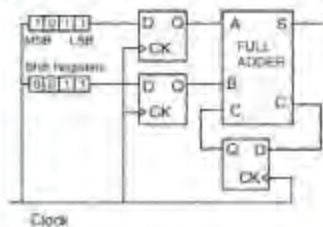
In the figure above, the ground has been shown by the symbol ∇ .

36. The power dissipation across the transistor Q1 shown in the figure is:
- 4.8 Watts
 - 5.0 Watts
 - 5.2 Watts
 - 0 Watts
37. If the regulated voltage increases by 20%, the power dissipation across the transistor Q1:
- increases by 20%
 - increases by 50%
 - remains unchanged
 - decreases by 20%
38. A new Binary Coded Pentary (BCP) number system is proposed in which every digit of a base-5 number is represented by its corresponding 3-bit binary code. For example, the base-5 number 24 will be represented by its BCP code 010100. In this numbering system, the BCP code 100010011001 corresponds to the following number in base-5 system:
- 423
 - 1324
 - 2201
 - 4231
39. An I/O peripheral device shown in the figure below is to be interfaced to a microprocessor. To select the I/O device in the I/O address range D4 H—D7 H, its 8085 chip-select (\overline{CS}) should be connected to the output of the decoder shown in the figure



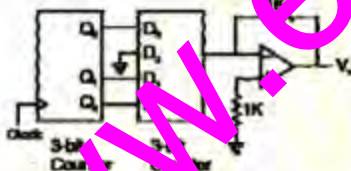
- a. output 7
- b. output 5
- c. output 2
- d. output 0

40. For the circuit shown in the figure below, two 4-bit parallel-in serial-out shift registers loaded with the data shown are used to feed the data to a full adder. Initially, all the flip-flops are in clear state. After applying two clock pulses, the outputs of the full adder should be

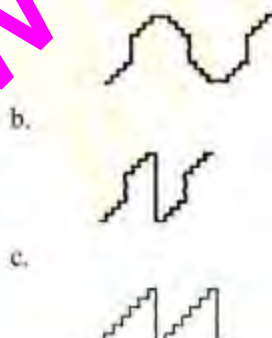


- a. $S = 0, C_0 = 0$
- b. $S = 0, C_0 = 1$
- c. $S = 1, C_0 = 0$
- d. $S = 1, C_0 = 1$

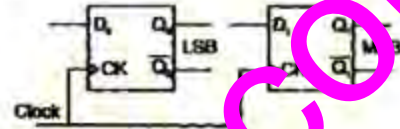
41. A 4-bit D/A converter is connected to a free-running 3-bit UP counter, as shown in the following figure. Which of the following waveforms will be observed at V_0 ?



In the figure shown above, the ground has been shown by the symbol ∇

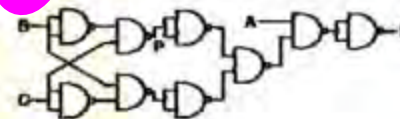


42. Two D-flip-flops, as shown below, are to be connected as a synchronous counter that goes through the following Q_1Q_0 sequence
 $00 \rightarrow 01 \rightarrow 11 \rightarrow 10 \rightarrow 00 \rightarrow \dots$
 The inputs D_0 and D_1 respectively should be connected as



- a. \bar{Q}_1 and Q_0
- b. \bar{Q}_0 and Q_1
- c. \bar{Q}_1Q_0 and \bar{Q}_1Q_0
- d. \bar{Q}_1Q_0 and Q_1Q_0

43. The point Pin the following figure is stuck-at-1. The output f will be



- a. \overline{ABC}
- b. \bar{A}
- c. ABC
- d. A

44. Consider the function $f(t)$ having Laplace transform

$$F(s) = \frac{\omega_0}{s^2 + \omega_0^2} \quad \text{Re}[s] > 0$$

The final value of $f(t)$ would be:

- a. 0
- b. 1
- c. $-1 \leq f(\infty) \leq 1$
- d. ∞

45. A signal $m(t)$ with bandwidth 500 Hz is first multiplied by a signal $g(t)$ where

$$g(t) = \sum_{k=-\infty}^{\infty} (-1)^k \delta(t - 0.5 \times 10^{-4} k)$$

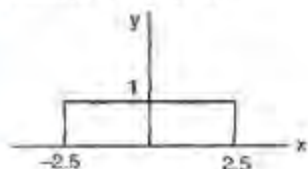
The resulting signal is then passed through an ideal low pass filter with bandwidth 1 kHz. The output of the low pass filter would be

- a. $\delta(t)$
 b. $m(t)$
 c. 0
 d. $m(t)\delta(t)$

46. A uniformly distributed random variable X with probability density function

$$f_x(x) = \frac{1}{10}(u(x+5) - u(x-5))$$

Where $u(\cdot)$ is the unit step function is passed through a transformation given in the figure below. The probability density function of the transformed random variable Y would be



- a. $f_y(y) = \frac{1}{5}(u(y+2.5) - u(y-2.5))$
 b. $f_y(y) = 0.5\delta(y) + 0.5\delta(y-1)$
 c. $f_y(y) = 0.25\delta(y+2.5) + 0.25\delta(y-2.5) + 0.5\delta(y)$
 d. $f_y(y) = 0.25\delta(y+2.5) + 0.25\delta(y-2.5) + \frac{1}{10}(u(y+2.5) - u(y-2.5))$

47. A system with input $x[n]$ and output $y[n]$ is given as $y[n] = \left(s + \frac{2}{1-n}\right)x[n]$. Then

system is

- a. Linear, stable and invertible
 b. Non-linear, stable and non-invertible
 c. Linear, stable and non-invertible
 d. Linear, unstable and invertible

48. Consider two transfer functions

$$G_1(s) = \frac{1}{s^2 + as + b} \text{ and}$$

$$G_2(s) = \frac{s}{s^2 + as + b}$$

The 3-dB bandwidths of their frequency responses are, respectively

- a. $\sqrt{a^2 - 4b}, \sqrt{a^2 + 4b}$
 b. $\sqrt{a^2 + 4b}, \sqrt{a^2 - 4b}$
 c. $\sqrt{a^2 - 4b}, \sqrt{a^2 - 4b}$

d. $\sqrt{a^2 + 4b}, \sqrt{a^2 + 4b}$

49. The unit-step response of a system starting from rest is given by

$$c(t) = 1 - e^{-2t} \text{ for } t \geq 0$$

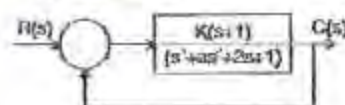
The transfer function of the system is

- a. $\frac{1}{1+2s}$
 b. $\frac{2}{2+s}$
 c. $\frac{1}{2+s}$
 d. $\frac{2s}{1+2s}$

50. The Nyquist plot of $G(j\omega)H(j\omega)$ for a closed loop control system, passed through $(-1, j0)$ point in the GH plane. The gain margin of the system in dB is equal to

- a. Infinite
 b. Greater than zero
 c. Less than zero
 d. Zero

51. The positive values of " K " and " a " so that the system shown in the figure below oscillates at a frequency of 2 rad/sec respectively are



- a. 1, 0.75
 b. 2, 0.75
 c. 1, 1
 d. 2, 2

52. The unit impulse response of a system is $h(t)e^{-t}, t \geq 0$

For this system, the steady-state value of the output for unit step input is equal to

- a. -1
 b. 0
 c. 1
 d. ∞

53. The transfer function of a phase-lead compensator is given by

$$G_c(s) = \frac{1+3Ts}{1+Ts} \text{ where } T > 0$$

The maximum phase-shift provided by such a compensator is

- a. $\pi/2$

- b. $\pi/3$
- c. $\pi/4$
- d. $\pi/6$

54. A linear system is described by the following state equation

$$\dot{X}(t) = AX(t) + BU(t), A = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

The state-transition matrix of the system is

- a. $\begin{bmatrix} \cos t & \sin t \\ -\sin t & \cos t \end{bmatrix}$
- b. $\begin{bmatrix} -\cos t & \sin t \\ -\sin t & -\cos t \end{bmatrix}$
- c. $\begin{bmatrix} -\cos t & -\sin t \\ -\sin t & \cos t \end{bmatrix}$
- d. $\begin{bmatrix} \cos t & -\sin t \\ \cos t & \sin t \end{bmatrix}$

Common Data for Questions 55 and 56:

Consider a unity-gain feedback control system whose open-loop transfer function is

$$G(s) = \frac{as + 1}{s^2}$$

55. The value of "a" so that the system has a phase-margin equal to 1.4 rad, is approximately equal to

- a. 2.40
- b. 1.40
- c. 0.84
- d. 0.74

56. With the value of "a" set for phase-margin of $\pi/4$, the value of unit-impulse response of the closed-loop system at $t = 1$ second is equal to

- a. 2.40
- b. 2.40
- c. 1.84
- d. 1.74

57. The minimum sampling frequency (in samples/sec) required to reconstruct the following signal from its samples without distortion

$$x(t) = 5 \left(\frac{\sin 2\pi 100t}{\pi t} \right)^3 + 7 \left(\frac{\sin 2\pi 1000t}{\pi t} \right)^2$$

would be

- a. 2×10^3

- b. 4×10^3
- c. 6×10^3
- d. 8×10^3

58. The minimum step-size required for a Delta-Modulator operating at 32K samples/sec to track the signal (here $u(t)$ is the unit-step function)

$x(t) = 125t(u(t) - u(t-1)) + (250 - 125t)(u(t-1) - u(t-2))$ so that slope-overload is avoided, would be

- a. 2^{-10}
- b. 2^{-8}
- c. 2^{-6}
- d. 2^{-4}

59. A zero-mean white Gaussian noise is passed through an ideal lowpass filter of bandwidth 10 kHz. The output is then uniformly sampled with sampling period $t_s = 0.05$ msec. The samples so obtained would be

- a. correlated
- b. statistically independent
- c. uncorrelated
- d. orthogonal

60. A source generates three symbols with probabilities 0.25, 0.25, 0.50 at a rate of 3000 symbols per second. Assuming independent generation of symbols, the most efficient source encoder would have average bit rate is

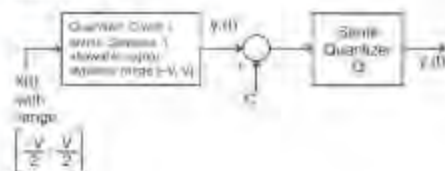
- a. 6000 bits/sec
- b. 4500 bits/sec
- c. 3000 bits/sec
- d. 1500 bits/sec

61. The diagonal clipping in Amplitude Demodulation (using envelop detector) can be avoided if RC time-constant of the envelope detector satisfies the following condition, (here W is message bandwidth and ω is carrier frequency both in rad/sec)

- a. $RC < \frac{1}{W}$
- b. $RC > \frac{1}{W}$
- c. $RC < \frac{1}{\omega}$
- d. $RC > \frac{1}{\omega}$

62. In the following figure the minimum value of the constant "C", which is to be added

to $y_1(t)$ such that $y_1(t)$ and $y_2(t)$ are different, is



- Δ
- $\frac{\Delta}{2}$
- $\frac{\Delta^2}{12}$
- $\frac{\Delta}{L}$

63. A message signal with bandwidth 10 kHz is Lower-Side Band SSB modulated with carrier frequency $f_{c1} = 10^6$ Hz. The resulting signal is then passed through a Narrow-Band Frequency Modulator with carrier frequency $f_{c2} = 10^9$ Hz.

The bandwidth of the output would be

- 4×10^4 Hz
- 2×10^6 Hz
- 2×10^9 Hz
- 2×10^{10} Hz

Common Data for Questions 64, 65:

Let $g(t) = p(t) * p(t)$, where $*$ denotes convolution and $p(t) = u(t) - u(t-1)$ with $u(t)$ being the unit step function

64. The impulse response of a filter matched to the signal $s(t) = g(t) + \delta(t-2) * g(t)$ is given as:

- $s(1-t)$
- $s(1-t)$
- $-s(t)$
- $s(t)$

65. An Amplitude Modulated signal is given as

$$x_{AM}(t) = 100(p(t) + 0.5g(t))\cos\omega_c t$$

in the interval $0 \leq t \leq 1$. One set of possible values of the modulating signal and modulation index would be

- $t, 0.5$
- $t, 1.0$
- $t, 2.0$
- $t^2, 0.5$

Common Data for Questions 66 & 67:

The following two questions refer to wide sense stationary stochastic processes

66. It is desired to generate a stochastic process (as voltage process) with power spectral density

$$S(\omega) = \frac{16}{16 + \omega^2}$$

by driving a Linear-Time-Invariant system by zero mean white noise (a voltage process) with power spectral density being constant equal to 1. The system which can perform the desired task could be

- first order low pass R-L filter
- first order high pass R-C filter
- tuned L-C filter
- series R-L-C filter

67. The parameters of the system obtained in Q.66 would be

- first order R-L low pass filter would have $R = 4\Omega$ $L = 1H$
- first order R-C high pass filter would have $R = 4\Omega$ $C = 0.25F$
- tuned L-C filter would have $L = 4H$ $C = 4F$
- series R-L-C low pass filter would have $R = 1\Omega$, $L = 4H$, $C = 4F$

Common Data for Questions 68 & 69:

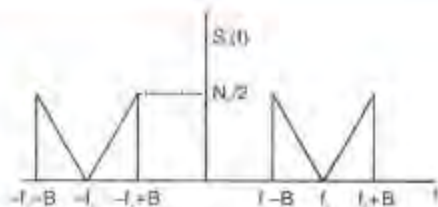
Consider the following Amplitude Modulated (AM) signal, where $f_m < B$:

$$x_{AM}(t) = 10(1 + 0.5 \sin 2\pi f_m t) \cos 2\pi f_c t$$

68. The average side-band power for the AM signal given above is

- 25
- 12.5
- 6.25
- 3.125

69. The AM signal gets added to a noise with Power Spectral Density $S_n(f)$ given in the figure below. The ratio of average sideband power to mean noise power would be:



- a. $\frac{25}{8N_0B}$
 b. $\frac{25}{4N_0B}$
 c. $\frac{25}{2N_0B}$
 d. $\frac{25}{N_0B}$

70. A medium of relative permittivity $\epsilon_{r2} = 2$ forms an interface with free-space. A point source of electromagnetic energy is located in the medium at a depth of 1 meter from the interface. Due to the total internal reflection, the transmitted beam has a circular cross-section over the interface. The area of the beam cross-section at the interface is given by

- a. $2\pi \text{ m}^2$
 b. $\pi^2 \text{ m}^2$
 c. $\pi/2 \text{ m}^2$
 d. $\pi \text{ m}^2$

71. A medium is divided into regions I and II about $x = 0$ plane, as shown in the figure below. An electromagnetic wave with electric field $E_1 = 4\hat{a}_x + 3\hat{a}_y + 5\hat{a}_z$ is incident normally on the interface from region-I. The electric field E_2 in region-II at the interface is



- a. $E_2 = E_1$
 b. $4\hat{a}_x + 0.75\hat{a}_y - 1.25\hat{a}_z$
 c. $3\hat{a}_x + 3\hat{a}_y + 5\hat{a}_z$
 d. $-3\hat{a}_x + 3\hat{a}_y + 5\hat{a}_z$

72. When a plane wave traveling in free-space is incident normally on a medium having $\epsilon_r = 4.0$, the fraction of power transmitted into the medium is given by

- a. $8/9$
 b. $1/2$
 c. $1/3$

d. $5/6$

73. A rectangular waveguide having TE_{10} mode as dominant mode is having a cutoff frequency of 18-GHz for the TE_{20} mode. The inner broad-wall dimension of the rectangular waveguide is

- a. $5/3 \text{ cms}$
 b. 5 cms
 c. $5/2 \text{ cms}$
 d. 10 cms

74. A mast antenna consisting of 50 meter long vertical conductor operates over a perfectly conducting ground plane. It is base-fed at a frequency of 600 MHz. The radiation resistance of the antenna in Ohms is

- a. $\frac{2\pi^2}{5}$
 b. $\frac{\pi^2}{5}$
 c. $\frac{4\pi^2}{5}$
 d. $10\pi^2$

75. In a microwave test bench, why is the microwave signal amplitude modulated at 1 kHz?

- a. To increase the sensitivity of measurement
 b. To transmit the signal to a far-off place
 c. To study amplitude modulation
 d. Because crystal detector fails at microwave frequencies

Common Data for Questions 76 & 77:

A 30-Volts battery with zero source resistance is connected to a coaxial line of characteristic impedance of 50 Ohms at $t = 0$ second and terminated in an unknown resistive load. The line length is such that it takes $400\mu\text{s}$ for an electromagnetic wave to travel from source end to load end and vice-versa. At $t = 400\mu\text{s}$, the voltage at the load end is found to be 40 Volts.

76. The load resistance is

- a. 25 Ohms
 b. 50 Ohms
 c. 75 Ohms
 d. 100 Ohms

77. The steady-state current through the load resistance is

- a. 1.2 Amps
 b. 0.3 Amps
 c. 0.6 Amps

78. d. 0.4 Amps
Following is the segment of a 8085 assembly language program:

```

                LXI SP, EFFFH
                CALL 3000H
3000H:         LXIH, 3CF4H
                PUSH PSW
                SPHL
                POP PSW
                RET

```

On completion of RET execution, the contents of SP is

- a. 3CFO H
b. 3CF8 H
c. EFFF H
d. EFFF H
79. The eigenvalues and the corresponding eigenvectors of a 2×2 matrix are given by

$$\lambda_1 = 8 \quad v_1 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$\lambda_2 = 4 \quad v_2 = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

The matrix is

- a. $\begin{bmatrix} 6 & 2 \\ 2 & 6 \end{bmatrix}$
b. $\begin{bmatrix} 4 & 6 \\ 6 & 4 \end{bmatrix}$
c. $\begin{bmatrix} 2 & 4 \\ 4 & 2 \end{bmatrix}$
d. $\begin{bmatrix} 4 & 8 \\ 8 & 4 \end{bmatrix}$
80. For the function of a complex variable $W = \ln Z$ (where, $W = u + jv$ and $Z = x + jy$), the $u = \text{constant}$ lines get mapped in Z -plane as

- a. set of radial straight lines
b. set of concentric circles
c. set of confocal hyperbolas
d. set of confocal ellipses
81. The value of the contour integral

$$\oint_{|z|=2} \frac{1}{z^2+4} dz \text{ in positive sense is}$$

- a. $j\pi/2$
b. $-\pi/2$
c. $-j\pi/2$
d. $\pi/2$
82. The integral $\int_0^\pi \sin^3 \theta d\theta$ is given by
- a. 1/2
b. 2/3

c. 4/3

d. 8/3

83. Three companies X, Y and Z supply computers to a university. The percentage of computers supplied by them and the probability of those being defective are tabulated below

Company	% of computers supplied	Probability of being defective
X	60%	0.01
Y	30%	0.02
Z	10%	0.03

Given that a computer is defective, the probability that it was supplied by X is

- a. 0.1
b. 0.2
c. 0.3
d. 0.4

84. For the matrix $\begin{bmatrix} 4 & 2 \\ 2 & 4 \end{bmatrix}$ the eigenvalue corresponding to the eigenvector $\begin{bmatrix} 101 \\ 101 \end{bmatrix}$ is

- a. 2
b. 4
c. 6
d. 8

85. For the differential equation $\frac{d^2 y}{dx^2} + k^2 y = 0$ the boundary conditions are

1. $y = 0$ for $x = 0$ and
2. $y = 0$ for $x = a$

The form of non-zero solutions of y (where m varies over all integers) are

- a. $y = \sum_m A_m \sin \frac{m\pi x}{a}$
b. $y = \sum_m A_m \cos \frac{m\pi x}{a}$
c. $y = \sum_m A_m x^{\frac{m\pi}{a}}$
d. $y = \sum_m A_m e^{\frac{m\pi}{a}}$

86. As x increased from $-\infty$ to ∞ , the function

$$f(x) = \frac{e^x}{1+e^x}$$

- a. monotonically increases
b. monotonically decreases
c. increases to a maximum value and then decreases
d. decreases to a minimum value and then increases