

KPCL (Mechanical Engineering – AE) GENERAL INSTRUCTIONS

Time: 2 hrs

Max. Marks: 100



- 1. The question paper contains 100 objective questions, each carrying **ONE** mark.
- 2. Answer all the questions. There is no negative marking.
- 3. Questions must be answered on a special machine gradable Objective Response Sheet (ORS) by darkening the appropriate oval (marked A, B, C, D). See box above.
- 4. Enter your application number on the left top side of the **ORS** by darkening the appropriate oval with a Black ink Ball-Point Pen.
- 5. Write your name and the application number on the right top side of the **ORS** in the specified locations in black ink and affix your signature in the box provided.
- 6. No charts or tables are provided in the examination hall. Calculators, cell phones and other types of electronic gadgets are strictly forbidden in the examination hall.
- 7. Use the blank pages provided at the end of the question paper for rough work. No extra sheets will be provided.
- 8. After completing the examination, you must hand over both the question paper and the **ORS** answer sheet to the invigilator.
- 9. A candidate found violating the instructions given above and/or those given by the invigilator, will be disqualified. Furthermore, a candidate giving assistance to any other candidate or seeking/receiving help from any source in answering questions or copying in any manner in the test, will forfeit his/her chance of being considered for selection.

1.	The infinite series $1 + x + \frac{x^2}{12} + \frac{x^3}{123} + \cdots$	··· corresponds to the follo	owing function:					
	(A) $\sin x$ (B) $\cos x$	(C) $\ln x$	(D) $\exp(x)$					
2.	An implicit relation between x and y is written $f(x,y) = 0$. It is known that $\partial f / \partial x = x^2 - ay$ and $\partial f / \partial y = y^2 - ax$. Then, $dy/dx =$							
	(A) $\frac{x^2 - ay}{y^2 - ax}$ (B) $\frac{x^2 - ay}{y^2 - ax}$	$(C) - \frac{x^2 - ay}{y^2 - ax}$	$(D) - \frac{y^2 - ax}{x^2 - ay}$					
3.	The slope of the tangent to the circle x (A) -1 (B) 0	$x^2 + y^2 = a^2$ at the point (1 (C) 1	,1) is: (D) √3					
4.	The parametric equations $x = a \cos \theta$ as (A) a parabola (B) an ellipse	nd $y = b \sin \theta$ represent: (C) a hyperbola	(D) a cycloid					
5.	If the function $f(x)$ is odd, then $\int_{-a}^{a} f(x)$)dx =						
	(A) $2\int_{0}^{a} f(x)dx$ (B) $2\int_{a}^{0} f(x)dx$	(C) 0	(D) $2\int_a^a f(x)dx$					
6.	The rank of the matrix $\begin{bmatrix} 2 & 4 & 8 \\ 1 & 2 & 1 \end{bmatrix}$ is:							
	(A) 0 (B) 1	(C) 2	(D) 3					
7.	The eigenvalues of the matrix $\begin{bmatrix} 1 & 3 \\ 2 & 2 \end{bmatrix}$	are:						
	(A) 1,-4 (B) -1,4	(C) 1,2	(D) 1,3					
8.	The solution of the differential equatio	$\sin \frac{d^2 y}{dx^2} + 4\frac{dy}{dx} + 4y = 0 (w$	with A and B denoting					
	constants) is: (A) $(A+Bx)\exp(-2x)$	(B) $(A + Bx) \exp(-2/$	x)					
	(C) $(A+Bx)\exp(2x)$	(D) $(A+Bx^2)\exp(2x)$)					
9.	The cartesian coordinates x and y are $x = r \cos \theta$ and $y = r \sin \theta$. The Jaco coordinates is:	related to the plane polar bian of transformation fr	coordinates r and θ as rom cartesian to polar					
	(A) $\cos\theta$ (B) $\sin\theta$	(C) $\tan \theta$	(D) <i>r</i>					
10.	The Laplace transform of sin(kt), with	usual notation, is:						
	k 12	k	2					

(A) $\frac{k}{s^2 - k^2}$ (B) $\frac{k^2}{s^2 - k^2}$ (C) $\frac{k}{s^2 + k^2}$ (D) $\frac{s}{s^2 - k^2}$

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11.	(A) surface in	ergence theorem relates a tegral (B) line integral	(C) contour integral	(D) differential
12.	The unit of ele (A) amperes	ctrical capacitance is: (B) volts	(C) joules	(D) farads
13.	Of the followin (A) wood	ng solid fuels, the fuel ha (B) anthracite coal	ving the largest calorific (C) bituminous c	value is: oal (D) peat
14.	One of the mean Temperature S (A) NTC therm (C) copper-cor	asuring instruments recor cale)-90 for calibration o nistor nstantan thermocouple	nmended by the ITS (Int of temperature is the: (B) platinum resistant (D) mercury-in-glass	ernational ce thermometer thermometer
15.	The pressure r steam and ice steam point an fixed points m (A) 273.149	ratio obtained from a con points is 1.3661. If the id ice points is divided in ethod is: (B) 273.160	nstant volume ideal gas absolute temperature d nto 100 degrees, the ice- (C) 373.149	thermometer between ifference between the point in K in this two (D) 373.160
16.	An ideal gas us due to the press index of comp (A) $x=1.4n$	ndergoes compression in ence of friction. If γ is th ression, then:	a compressor. The comp e ratio of specific heats a (C) = x < x	pression is irreversible and n is the polytropic
17.	Methane gas is an absolute pr contained in th (A) 12	s stored in a cylinder of c essure of 250 bar. Assur e cylinder in kg is: (B) 24	apacity 80 litres at a tem ning ideal gas behaviou (C) 36	perature of 300 K and r, the mass of the gas (D) 48
18.	The thermodyn state points. The 3-4 and 4-1, re (A) perpetual n (C) heat engine	namic cycle of a device i he heat interactions in kJ spectively. The device is notion machine-1 e	s 1-2-3-4-1, the numeral are 0, -100, 0 and 50 in a: (B) perpetual motion (D) refrigerator	s denoting the various the processes 1-2, 2-3, machine-2
19.	The ratio of spolytropic pro Q and the work	specific heats of a perfected a perfected by the polytropic exposed of the polytropic exposed by the process of	ect gas is γ . The gas upper the data of p is the relation of p . The relation is:	ndergoes a reversible on between heat input
	(A) $Q = \frac{\gamma - n}{\gamma - 1}$	$W \qquad (B) \ W = \frac{\gamma - n}{\gamma - 1}Q$	(C) $Q = \frac{n-\gamma}{\gamma-1}W$	(D) $W = \frac{n-\gamma}{\gamma-1}Q$
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20.	A three-stage reciprocating air compre- stages has an overall pressure ratio of 64.	ssor with perfect interco For minimum work input	boling between the it, the pressure ratio
	(A) 2 (B) 4	(C) 8	(D) 16
21.	In a jet-propulsion engine of an airplane of the combustion gases to the nozzle is velocity of 500 m/s. Neglecting the mass (A) 10 (B) 25	flying at a speed of 900 s 40 kg/s. The gases leav of fuel, the thrust on the (C) 40	kmph, the flow rate te the nozzle with a plane in kN is: (D) 900
22	Natural gas that does not contain hydroge	en sulphide is often called	1:
22.	(A) dry gas (B) sour gas	(C) sweet gas	(D) wet gas
23.	In an Orsat apparatus used for flue gas ar acid acts as:	halysis, the alkaline soluti	on of pyrogallic
	(A) CO absorber (B) CO ₂ absorber	(C) O ₂ absorber	(D) N ₂ absorber
24.	A flue gas analyzer shows the presence of fuel is known to contain 82.5% carbon by	of 80% N_2 and 10% CO_2 by mass, the air-fuel ratio is	by volume. If the s:
	(A) 10 (B) 15	(C) 20	(D) 25
25.	The air standard efficiency of an Otto cyc (A) 36.5% (B) 46.5%	cle with a compression ra (C) 56.5%	tio of 8 is: (D) 66.5%
26.	A better basis of comparison for a moder (A) Diesel cycle (B) Dual cycle	n high-speed oil engine i (C) Stirling cycle	s: (D) Otto cycle
27.	Cetane number is the percentage of cetan (A) cetane and methyl pyrrolidinone	(B) cetane and acetyler	of: ne
	(C) cetane and α -methyl naphthalene	(D) cetane and n-hepta	ne
28.	The volumetric efficiency of engines at h (A) stratification of charge	igh speeds can be improv (B) fuel injection	ved by:
	(C) the use of multiple cylinders	(D) supercharging	
29.	In a dual-combustion cycle, combustion partly at:	takes place partly at cons	tant volume and
	(A) constant temperature	(B) constant pressure	
	(C) constant enthalpy	(D) constant internal en	ergy
30.	The critical pressure ratio for a gas flow the nozzle inlet pressure is10 bar, the bac (A) 5.5 kPa (B) 10 kPa	wing through a converge ck pressure required to ch (C) 100 kPa	nt nozzle is 0.55. If oke the nozzle is: (D) 550 kPa

31.	The mass flow rat more than that cal (A) wet steam flow	e of steam through a co culated with equilibrium ws through the nozzle	m flow assumption. This means that: (B) supersaturated expansion is occurring				
	(C) water droplets	are freezing	(D) fog formation is	occurring			
32.	The ratio of the av during the same p (A) demand factor	verage load on a power eriod is called: r (B) capacity factor	plant over a certain period to the peak load (C) load factor (D) common factor				
33.	The term "attemp (A) tempering of	eration" refers to: superheater tubes	(B) reduction of the	steam temperature			
	(C) cleaning of flu	ue gas	(D) reduction in the	flue gas temperature			
34.	The deaerator in a concentraton of:	The deaerator in a steam power plant reduces the oxygen in the feed water to a concentraton of:					
	(A) 0.005 mL/L	(B) 0.05 mL/L	(C) 0.5 mL/L	(D) 5 mL/L			
35.	Supercritical boile (A) 0.22 bar	ers operate at an absolut (B) 2.2 bar	te pressure in excess (C) 22 bar	of: (D) 220 bar			
36.	From compactnes suitable:	s considerations, the fo	llowing type of air pr	eheater is the most			
	(A) plate type	(B) tubular type	(C) rotary type	(D) double-pipe type			
37.	The mass of coolid steam condensed	ing water in kg required is typically in the range	d in the condenser of	a power plant per kg of			
	(A) 10-25	(B) 30-45	(C) 50-65	(D) 75-100			
38.	The absolute pres steam is 4 kPa. Th	sure in a steam condens ne mass of air per unit n	ser is 7 kPa and the sa nass of steam is:	aturation pressure of			
	(A) 0.7	(B) 0.9	(C) 1.2	(D) 1.5			
39.	The pressure in a height in the follo	a column of isotherma wing manner:	l ideal gas in gravita	tional field varies with			
	(A) quadratic	(B) cubic	(C) sinusoidal	(D) exponential			
40.	In the troposphere (A) it decreases co	e, the variation of the prontinuously	ressure with height is (B) it first increases	such that: and then decreases			
	(C) it first decreases and then increases (D) it remains constant						
41.	A barge of weight water displaced in	t 196.2 kN floats in wat n^3 is:	ter of density 1000 kg	/m ³ . The volume of			
	(A) 1.962	(B) 10	(C) 20	(D) 196.2			

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- 42. In a vortex created in a real fluid, it is most likely that:
 - (A) the entire vortex is a forced vortex

(B) the entire vortex is a free vortex

- (C) the central portion is a free vortex and the remaining portion is a forced vortex
- (D) the central portion is a forced vortex and the remaining portion is a free vortex
- 43. In experimental work, the following method can be used to find the dimensionless numbers among which a functional relationship exists:
 (A) Rayleigh's method
 (B) Weighted residuals method
 (C) Finite element method
 (D) Sub-domain method
- 44. The flow of a liquid of density 1000 kg/m³ in a pipe of 0.1 m diameter with an average velocity of 1 m/s is dynamically similar to a gas of density 1 kg/m³ flowing in a 1.0 m diameter tube. The dynamic viscosities of the liquid and gas are respectively 10⁻³ Pa.s and 2×10⁻⁵ Pa.s. The average velocity of the gas in m/s is:
 (A) 0.1 (B) 2 (C) 15 (D) 100
- 45. In a fully developed pipe flow, the boundary layer thickness is equal to the:
 (A) diameter of the pipe
 (B) length of the pipe
 (C) radius of the pipe
 (D) square of the pipe radius
- 46. A source of disturbance moves at supersonic speed in a medium. If the Mach number is *M*, the semi-angle of the Mach cone is:
 (A) sin⁻¹(1/M) (B) sin⁻¹(M) (C) tan⁻¹(1/M) (D) tan⁻¹(M)
- 47. The head available for a turbine is $H = H_g$ -h, where H_g is the fixed gross head and $h=AQ^2$ is the friction head in the penstock, where A is a constant and Q is the volume flow rate of water through the system. The turbine water power P=BQH, where B is a constant. For maximum water power, the friction head should be: (A) $H_g/5$ (B) $H_g/4$ (C) $H_g/3$ (D) $H_g/2$
- 48. In a Pelton turbine, the mean bucket speed is 30 m/s. The net head available for the turbine in m is approximately:
 (A) 90 (B) 120 (C) 150 (D) 180
- 49. The operating speed of a turbine is 625 rpm. Its unit speed is 125 rpm. The turbine head in m is:
 (A) 5 (B) 25 (C) 125 (D) 625
- 50. An axial flow turbine with variable pitch blades is:(A) Kaplan turbine (B) Pelton wheel (C) Propeller turbine (D) Radial turbine

51.	For a given power by the following	er, speed and head, the quantity:	e shape of a hydraulic	turbine runner is decided		
	(A) head coeffic	ient	(B) flow coefficient	nt		
	(C) specific spee	d	(D) power coeffici	ent		
			n hursh ng ditte M			
52.	A centrifugal pur head of 250 m, is	mp running at $1000\sqrt{2}$ s to be replaced by fou	rpm and handling 0.2 r similar pumps in ser	25 m ³ /s of water against a ies. The speed of each		
	(A) 500	(B) 700	(C) 800	(D) 900		
53.	The principle which carrying direct lo	hich states that the str bading can be consider	ess distribution over t ed uniform except at t	the cross-section of a bar the extreme ends is:		
	(A) Tresca's prir	nciple	(B) Unwin's princ	iple		
	(C) Soderberg's	principle	(D) Saint Venant's	s principle		
54.	In a tensile test of the relation betw $F = 125 \delta$. The Y (A) 125	of a specimen of length teen the load F (kN) ar Young's modulus of th (B) 200	a 200 mm and cross-see ad the elongation δ (m e material in kN/mm ² (C) 250	ectional area 125 mm ² , m) is found to be is: (D) 400		
55.	In a tensile test maximum load i 40 mm^2 . The ultimeter (A) 0.25	on a specimen with s found to be 60 kN. T imate tensile strength o (B) 0.5	original cross-section The cross-sectional are of the material in kN/n	al area of 120 mm ² , the ea at the time of failure is nm^2 is:		
	(11) 0.25	(D) 0.5	(0) 2.0	(D) 5.0		
56.	The following st (A) 0.2% proof s	ress may be taken as re stress	epresentative of the el (B) 10% of ultima	astic limit for copper: te stress		
	(C) 0.1% of yield	d stress	(D) 50% of failure	stress		
57.	when a steel bar the side of the sq	of cross-section 50 m juare decreases by 0.00	m × 50 mm is subjected 2 mm. If the Poisson	ed to a tensile loading, 's ratio is 0.25, the		
	(A) 16×10 ⁻⁵	(B) 0.002	(C) 50	(D) 2500		
58.	A bar is held bet	ween rigid planes and	is heated by 50°C. If t	he coefficient of linear		
	expansion of the (A) 10^{-5}	bar material is 10^{-5} pe (B) 50×10^{-5}	r °C, the compressive (C) 50	strain in the bar is: (D) 50×10^5		
59.	A bar with a cross-sectional area 400 mm ² is subjected to an axial pull of 4000 N. The normal stress in N/mm ² on a plane making an angle of 60° with the axis is: (A) 2.5 (B) 400 (C) 2000 (D) 4000					
60.	A bar is subjecte	d to an axial stress of the st	50 N/mm^2 . The maximed to the axis is:	num shear stress in		
	(A) 12.5	(B) 25	(C) 50	(D) 100		

A rectangular metal plate with its two sides parallel to x-axis and the other two sides 61. parallel to y-axis is subjected to a tensile stress of 45 MPa in x-direction and to a compressive stress of 20 MPa in y-direction. If the Young's modulus for the plate material is 200×10^3 MPa and the strain in the x-direction is 25×10^{-5} , the Poisson's ratio is: (D) 0.25

(C) 0.2 (A) 0.1 (B) 0.15

- A compressed air cylinder has an internal diameter of 2 m and a wall thickness of 10 62. mm. If the allowable stress both in the longitudinal and circumferential directions is 50 MPa, the safe gauge pressure in MPa is: (D) 50 (A) 0.5 (B) 2 (C) 10
- The relation between the sagging bending moment (in kN.m) and the distance x (in 63. m) measured from one end of a loaded beam is given by $M = -(x^3/6) - 5x^2 + 500(x/3)$. The magnitude of the intensity of loading in kN/m at x=10 m is: (B) 15 (C) 20 (D) 25 (A) 10
- The relation between the bending moment M and the shear force F for a loaded beam, 64. with x measured along the length of the beam, is given by: (D) $F = d^2 M/dx^2$ (A) M = dF/dx(B) $M = d^2 F/dx^2$ (C) F = dM/dx
- A simply supported beam with uniformly distributed load has equal overhangs at 65. either end. The ratio of each overhang length to the beam length for the magnitudes of the bending moments at the supports and at the centre of the beam to be equal is about:
 - (C) one-fifth (D) one-sixth (B) one-fourth (A) one-third
- A solid of cube shape is subjected to equal tensile stresses along three mutually 66. perpendicular directions parallel to the sides. The strain in each direction is found to be 3×10^{-5} . If the side of the cube is 30 mm, the change in the volume of the solid is: $(A) 10^{-6}$ (B) 9×10^{-4} (C) 0.09 (D) 0.81
- A beam loaded as shown in the figure is 67. supported at A and B. With distance measured from the end A, the bending moment at the section XX in kN.m is: (B) -5 50 kN (A) -10 (D) 10 (C) -2
- The bending moment in the span x=0 to x=0.5L of a beam is 0.5Px. If the beam is 68. supported at x=0 and has maximum deflection at x=0.5L, the deflection at x=0.5L, with usual notation, is: (C) $PL^{3}/(36EI)$ (D) $PL^{3}/(48EI)$ (B) $PL^{3}/(24EI)$ (A) $PL^{3}/(16EI)$

- 69. The two ends of a long metallic strip of thickness 2 mm are bent and clamped together to form a circular ring of mean radius 0.8 m. If the Young's modulus of the material of the strip is 200 GPa, the maximum bending stress in the strip in MPa is:
 (A) 200 (B) 250 (C) 450 (D) 500
- 70.A short concrete column of circular cross-section with diameter D carries a
compressive load off-centre from the axis, at a radius R. If the column cannot
withstand tensile stress, the maximum permissible value of R is:
(A) D/64 (B) D/32 (C) D/16 (D) D/8
- 71. The bending moment in the span x=0 to x=0.5L of a beam is 0.5Px. If the beam is supported at x=0 and has maximum deflection at x=0.5L, the slope at x=0.5L, with usual notation, is:
 (A) PL²/(16EI) (B) PL²/(24EI) (C) PL²/(36EI) (D) PL²/(48EI)
- 72. The area of the bending moment diagram for a loaded cantilever is 192 square units. The centroid of the diagram is at a distance of 3 units from the free end. If the flexural rigidity is *EI*, the deflection at the free end in consistent units is:
 (A) 1/(576EI) (B) 1/(64EI) (C) 64/(EI) (D) 576/(EI)
- 73. A circular shaft transmitting torque has solid cross-section for some length and hollow cross-section for the rest of the length. If subscripts 1 and 2 denote the solid and hollow portions, L is the length, J is the polar moment of inertia and G is the torsional modulus, the twist per unit torque is:
 (A) J₁/(L₁G₁)+ J₂/(L₂G₂)
 (B) G₁/(L₁J₁)+ G₂/(L₂J₂)

(c) $L_1/(J_1G_1) + L_2/(J_2G_2)$ (c) $L_2/(J_1G_1) + L_1/(J_2G_2)$ (c) $L_2/(J_1G_1) + L_1/(J_2G_2)$

- 74. Torque is transmitted to different machines from the two ends of shaft, while the drive torque is applied at an intermediate section. If subscripts 1 and 2 denote the circular shaft portions on either side of the intermediate section, L is the length and J is the polar moment of inertia, the condition for the transmitted torques to be equal is: (A) $J_1/J_2=(L_1/L_2)^{0.5}$ (B) $J_1/J_2=L_1/L_2$ (C) $J_1/J_2=(L_1/L_2)^2$ (D) $J_1/J_2=(L_1/L_2)^4$
- 75. Two helical springs of the same material have the same number of coils and the same coil diameter. The wire diameter of the first spring is twice that of the second. The ratio of the deflection of the first spring to that of the second, for the same load, is:
 (A) 1/16 (B) 1/8 (C) 8 (D) 16
- 76. A helical spring undergoes a deflection of 10 mm under a load of 50 kN. A second spring undergoes a deflection of 5 mm for the same load. The stiffness in kN/mm of the series combination of the springs is:
 (A) 3.3 (B) 5.0 (C) 10.0 (D) 15.8

- 77. In a tension test, a specimen of gauge length 50 mm with original cross-sectional area 120 mm² fails at a load of 60 kN. The cross-sectional area at the time of failure is 40 mm². The ultimate tensile strength of the material in kN/mm² is:
 (A) 0.5 (B) 1.5 (C) 2.0 (D) 3.0
- 78. A truck negotiates a curve of mean radius R. The coefficient of friction between the wheels and the road is μ . If g is the gravitational acceleration and the plane of the road is horizontal, the speed of the truck above which the truck skids is: (A) $(\mu g R)^{0.25}$ (B) $(\mu g R)^{0.5}$ (C) $\mu g R$ (D) $(\mu g R)^2$
- 79. The mean transverse distance between the tyres of a car is 1.2 m and the centre of gravity of the car is 1.6 m above the plane of the road. If, during negotiating a curve at high speed, skidding of the car is preferable to overturning, the coefficient of friction between the tyres and road should be less than:
 (A) 0.56 (B) 0.75 (C) 1.33 (D) 1.77
- 80. A rope fastened to a mass of M kg is passed over a pulley and is drawn such that the mass accelerates upwards with an acceleration of $a \text{ m/s}^2$. The gravitational acceleration is $g \text{ m/s}^2$. The tension in the rope in N is: (A) Mg(g-a)/a (B) Ma(a+g)/g (C) M(a+g) (D) M(a-g)
- 81. The figure shows a reciprocating engine mechanism with the required data. The rotational speed of the crank OB in rpm is:



- B 0.5 m 45° 0 0 A 1.2 m/s 1.2 m
- 82. In the figure shown, AB is a link of length 4 m, with the ends A and B constrained to move along the vertical and horizontal directions, respectively. If at a certain instant, the velocity of A is $2\sqrt{2}$ m/s downwards as shown, the magnitude of the velocity in m/s of C, which is the mid-point of AB, is:





83. The mean rotational speed of a flywheel of 200 kg.m² mass moment of inertia is $300/\pi$ revolutions per minute. If the coefficient of speed fluctuation is 5%, the energy fluctuation of the flywheel in kJ is: (A) 2 (B) 2π (C) 200 π (D) 300

84.	A vertical screw for raising weights has a single-start square thread, a pitch of 10 mm and a mean diameter of 50 mm. If the coefficient of friction is 0.15, the ratio of the force applied at the mean thread radius to the weight raised is: (A) 0.055 (B) 0.11 (C) 0.22 (D) 0.44					
85.	A conical pivot type thrust bearing is is cone angle of 60° and with the intrespectively. The pressure in kPa, cons when the bearing supports a load of 30 (A) 100.0 (B) 283.7	n the form of a frustum of a cone with a semi- ner and outer radii 100 mm and 200 mm, sidered to be uniform over the bearing surface, kN, is: (C) 300.0 (D) 318.3				
86.	Two geometrically identical slabs have The thermal conductivity of slab-1 i temperature difference in slab-1 to that (A) 1/4 (P) $1/2$	the same heat flux across their thickness. s four times that of slab-2. The ratio of the in slab-2 is: (C) 2				
	(A) 1/4 (B) 1/2	(C) 2 (D) 4				
87.	LMTD in case of counter flow heat exchanger:	(R) is lower				
	(C) is the same	(D) depends on the area of heat exchanger				
	(C) is the same	(D) depends on the area of heat exchanger				
88.	The units of Stefan-Boltzmann constant (A) $W/(m^2 K)$ (B) $W/(m^4 K)$	t are: (C) $W^2/(m K^4)$ (D) $W/(m^2 K^4)$				
89.	 In free convection heat transfer, the Nusselt number is a function of : (A) Grashof number and Reynold number (B) Grashof number and Prandtl number (C) Prandtl number and Reynold number (D) Grashoff number, Prandtl number and Reynold number 					
90.	A common process by which food cans (A) blanking (B) spinning	are produced is: (C) deep-drawing (D) machining				
91.	Typical deformation velocities in m/s in (A) 0.005 (B) 0.05	n a forging process are of the order of: (C) 0.5 (D) 5				
92.	The true density of a moulding sand kg/m^3 . The porosity of the moulding sa	is 2650 kg/m ³ and the bulk density is 1600 and is: $(D) = 0.5$				
	(A) 0.3 (B) 0.4	(C) 0.5 (D) 0.6				
93.	The blow holes in a solidified steel ing gas:	ot are caused by the release of the following				
	(A) CO (B) CO ₂	(C) N_2O (D) NO_2				

94.	Nitriding of an all	loy steel is:				
	(A) an annealing process		(B) a tempering process			
	(C) a case harden	ing process	(D) a recrystallizat	ion process		
95.	The operation of producing a conical surfa (A) end cutting (B) countersinking		rface at the end of a h (C) counterboring	ole is called: (D) fractional drilling		
96.	If the recommend the rotational spe	led cutting speed to dri ed of the drill in revolu	ll a 10 mm hole in a i itions per minute is:	l a 10 mm hole in a material 25 m/min, then tions per minute is:		
	(A) 100	(B) 250	(C) 564	(D) 625		
97.	A tap is used for (A) gear teeth	producing: (B) internal threads	(C) tapered holes	(D) square holes		
98.	The main advantage of a horizontal band saw is:					
	(A) the good surf	ace finish	(B) the smaller am	(B) the smaller amount of heat produced		
	(C) the minimum wastage of material		(D) the minimum maintenance cost			
99.	The process by w multiple-tooth cu	which material is removing tool is called:	ved by feeding a work	piece against a rotating		
	(A) milling	(B) drilling	(C) boring	(D) reaming		
100.	With reference to (A) diameter of t	a grinding wheel, the	term wheel structure refers to the:			
	(C) this lange of	the wheel	(D) share a file and asl			
	(C) thickness of	the wheel	(D) snape of the wheel			

End of the Question Paper

A &. (Mech) R'Senios

Answer Key of AEM-

QNO.	ANS	QNO.	ANS	QNO.	ANS	QNO.	ANS	
1	D	26	D	51	С	76	A	==
2	С	27	С	52	A	77	в	
3	A	28	D	53	D	78	в	
4	в	29	в	54	в	79	в	
5	С	30	D	55	в	80	С	
6	С	31	в	56	A	81	в	
7	в	32	С	57	A	82	в	
8	A	33	в	58	D	83	A	
9	D	34	A	59	A	84	в	
10	С	35	D	60	A	85	D	
11	A	36	С	61	D	86	A	
12	D	37	D	62	A	87	A	
13	в	38	С	63	С	88	D	. 1
14	в	39	D	64	A	89	в	
15	A	40	A	65	С	90	С	
16	D	41	С	66	D	91	D	
17	A	42	D	67	С	92	в	×
18	D	43	A	68	D	93	A	
19	С	44	в	69	в	94	С	
20	в	45	С	70	D	95	в	
21	A	46	A	71	D	96	С	
22	С	47	С	72	D	97	в	
23	С	48	D	73	С	98	С	
24	D	49	в	74	в	99	A	
25	С	50	A	75	A	100	в	

Verified With original any